

1 **Research Article**

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3 **Tattoo-like Epidermal Electronics as Skin Sensors for Human Machine**
4 **Interfaces**

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29 **How to cite this article:** Wong T, Yiu C, Zhou J, Song Z, Liu Y, Zhao L, Yao K,
30 Park W, Yoo W, Song E, Xie Z, Yu X. Tattoo-like Epidermal Electronics as Skin
31 Sensors for Human Machine Interfaces. *Soft Sci* 2021;1:[Accept].
32 <https://dx.doi.org/10.20517/ss.2021.09>

33

34 **Received:** 30 Jul 2021 **Revised:** 22 Sep 2021 **Accepted:** 23 Sep 2021 **First online:**
35 23 Sep 2021

36

37

38 **Abstract**

39 Flexible electronic skin (e-skin) has been proved for their diverse applications in
40 prosthesis sensing, body-motion monitoring, and the human-machine interfaces, due
41 to their superior mechanical properties and commendable electrical characteristics.
42 However, the reported e-skins are still relatively thick($>10\mu\text{m}$) and uncomfortable for
43 long-term use on the human body. Herein, an ultra-thin, skin-integrated designs of
44 strain sensor with miniaturized dimensions, based on the piezoresistive effect, with
45 excellent stability and robustness are introduced. Fractal curve-shaped Au electrode in
46 a serpentine format, which is the dominant component of the strain sensor, is sensitive
47 to the ambient strain variation and able to turn the mechanical motion into stable
48 electrical signal output. With the advanced design of the metallic electrodes, the
49 device presents good operational stability and excellent mechanical tolerance towards
50 bending, stretching, and twisting. The stain sensor allows intimate mounting onto the
51 human epidermal surface for detecting body motions. By adopting the liquid bandage
52 (LB) as the encapsulation layers, the device owns an ultrathin thickness ($6.2\ \mu\text{m}$),
53 high sensitivity towards mechanical deformations, which is able to clearly detect
54 motions such as walking, finger bending, and human pulse rate with identifiable
55 electrical signals. Furthermore, the tattoo-like strain sensor is applied in robotic
56 control by tracing finger bending motion and result in smooth control of a robotic
57 hand nearly without any detention. The e-skin has exhibited a great potential in
58 wearable electronics and the human-machine interfaces.

59

60 **Keywords:** Skin-integrated electronics, ultrathin, excellent repeatability, fractal
61 design, stretchable electronics.

62

63 INTRODUCTION

64 Recently, epidermal electronics have attracted much attention around the world for its
65 excellent mechanical properties and electronic characteristics[1-10]. Up to now,
66 extensive flexible strain sensors have been developed based on various operational
67 principles, such as piezoelectricity[11-14], triboelectricity[15-17], piezoresistance[18-
68 21][22], e.g. Among the reported strain sensors, piezoelectric and triboelectric devices
69 have raised extremely high interests for their natural characteristics in self
70 powering[23-31]. However, the instantaneous electrical signals and fast attenuation of
71 electrical performance significantly limits their further development in the application
72 of e-skin[32]. Distinguished with the self-powered strain sensors, e-skin, based on
73 piezoresistive effect, provides functions closer to human skin, capable of real-time
74 detecting strain variations accurately[33-38]. Resistance change of the piezoresistive
75 in e-skin can be conveniently transformed into voltage changes via real-time electrical
76 monitoring of the sensor, then recognized by microcontroller for later robotic control.

77 Benefited from the fast development of materials science, many piezoresistive effect-
78 based e-skins have been reported by incorporating advanced conductive materials,
79 such as graphene and PDMS composite[39-42], ionic conductive hydrogels[43-45],
80 graphene coated fabric[46-48], e.g. To achieve sufficient repeatability and stability,
81 the fabrication process of the newly-developed materials tends to require expensive
82 equipment and rigorous experimental environment, difficult with standard facilities in
83 academic cleanrooms. Compared to these strain sensors, e-skins based on metal
84 electrodes can realize a low-cost fabrication but high stability and repeatability with
85 sufficient electrical sensitivity[48]. As the noble metal, gold (Au) exhibits high
86 oxidation resistance, suitable for fabricating the strain sensor.[49, 50] To realize the
87 long-term utilization on the human skin surface, e-skin should fulfill several
88 characteristics, including 1) extremely light-weight and imperceptible architectures
89 without any limitation and influence on body motion. 2) skin-compatible interfaces to
90 the targeted skin with a soft, curved dynamic surface in a stable, safe fashion, not easy

91 to split away off skin surface. 3) outstanding operational performance characteristics
92 with high sensitivity and accuracy.

93

94 Herein, we report an ultrathin skin-integrated strain sensor based on the piezoresistive
95 effect with excellent stability and repeatability. The key component is the Au
96 electrode in the format of fractal curve, sensitive to the ambient strain variations. To
97 minimize the effect of the device on the skin strain field distribution, the overall size
98 of the sensor is designed as $5\text{ mm} \times 2\text{ mm} \times 6.2\text{ }\mu\text{m}$ (length \times width \times thickness) with
99 a light weight of 0.204 mg. Compared with the conventional strain sensor based on
100 piezoresistive effect, our strain sensor demonstrates superiorly tiny size and thin
101 thickness with competitive stretching range and sensitivity (**Table S2**).^[51-56] Guided
102 by theoretical modeling, the advanced structure design enables conformal integration
103 with the skin under large mechanical deformations. In order to yield the intimate
104 contact on complex textures of epidermal surfaces, liquid bandage is sprayed as a
105 connection layer between the sensors and the epidermal surface. Compared to the
106 commonly adopted PDMS layer, the liquid bandage owns the advantages of thin
107 thickness (1 μm), and light weight. The tight bondage between the sensors and the
108 epidermal surface allows the users' unhindered movements and providing precise
109 measurement of the body motions sensing in an highly accurate approach. By
110 accurately capturing finger motions and pulse rate, the sensor provides a promising
111 alternative for real-time monitoring human health. In addition, with signals obtained
112 from the strain sensors, a six-degree-of-freedom prosthetic arm is then used to imitate
113 the motion of the human hand, by applying to program for sensitivity and detection
114 adjustment.

115

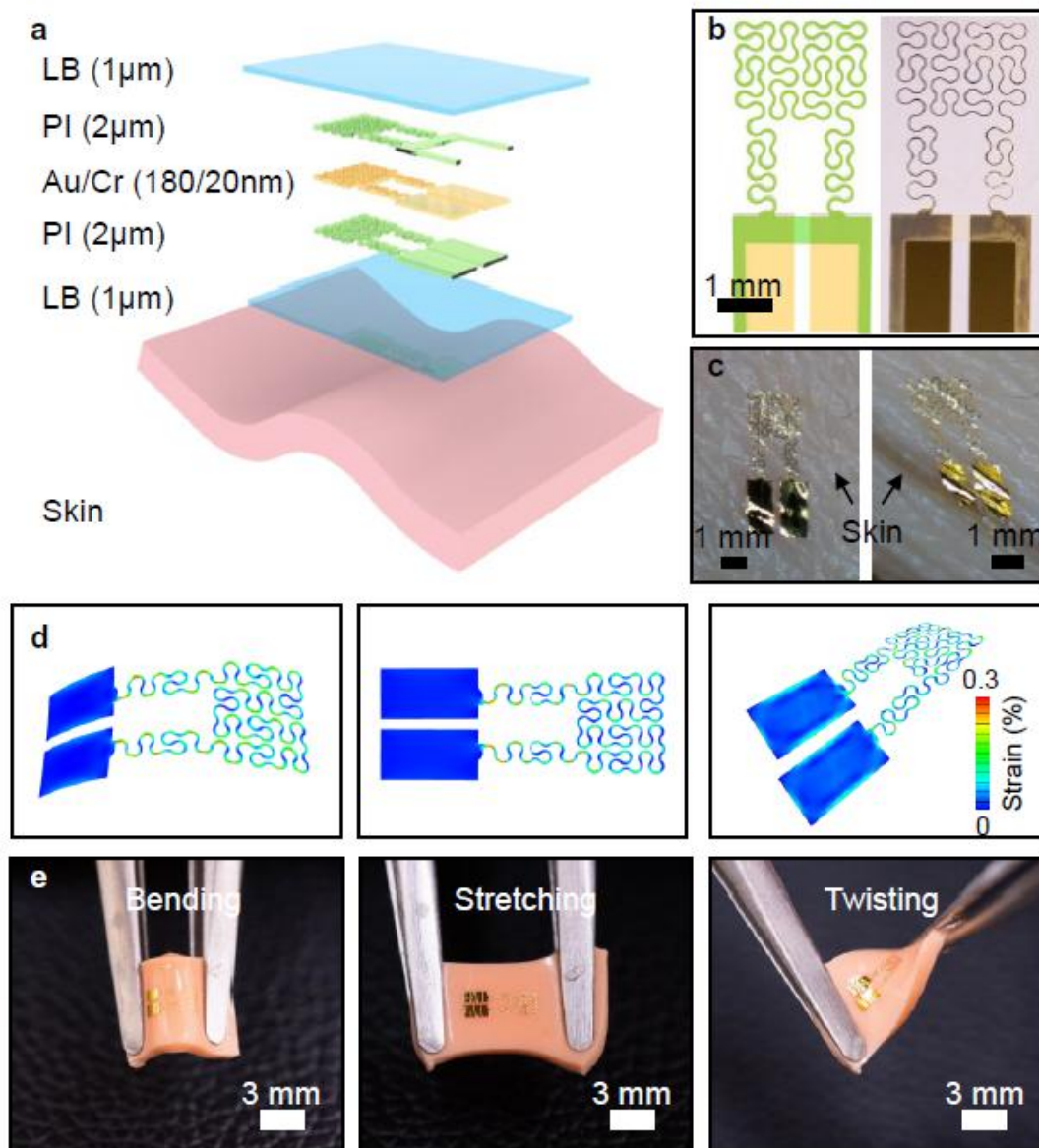
116 **DISCUSSION AND RESULT**

117 **Fig. 1a** presents the schematic diagram of the strain sensor. To ensure the surface
118 smoothness and the fabrication compatibility, a quartz glass was used as the substrate
119 first, with a spin coated Poly(methyl methacrylate) (PMMA) thin film on top as
120 sacrificial layer and a thin polyimide (PI) film as metal electrode supporting layer.
121 Metallic layers (Cr/Au) were deposited on the PI and patterned by photolithography,
122 serving as the functional electrode for strain change detection. Spin-casting another PI

123 and selectively dry etching by Reactive Ion Etching (RIE) provided a top
124 encapsulation layer for building a robust system. Dissolving the PMMA with acetone
125 enabled transfer printing of the electrode onto the targeted skin area with pre-sprayed
126 liquid bandage through a water-soluble tape (WST). Finally, an additional layer of
127 liquid bandage was sprayed on top of the electronics to encapsulate the exposed gold
128 electrode. The device features by the filamentary fractal design of the gold electrode
129 (200 nm) and an ultrathin and stretchable encapsulation layer (liquid bandage, 1 μm)
130 to enhance the overall flexibility and biaxial stretchability of the system (**Fig. 1b**).
131 The liquid bandage acts as a tight adhesion and robust encapsulation of the strain
132 sensor. A sensor is mounted on a volunteer's forearm over 12 hours, during the period,
133 the volunteer is allowed to perform any daily movements, like walking, running, and
134 twisting his forearm. After 12 hours, the sensor is still mounted on his forearm and
135 there is not any sign of flaking. According to the experimental studies, the ultrathin
136 encapsulation layers can provide an excellent protection of the gold electrode
137 underneath, and the sensor could endure various mechanical forces, like continuous
138 rubbing, while remaining undamaged (**Movie S1**). Apart from the external loads, the
139 liquid bandage is waterproof, which could protect the sensor in the moisture
140 environment. There is experimental study proves that, with the encapsulation of the
141 liquid bandage, the sensor is approximately unaffected in a watery environment,
142 where the change in the electrical signal ($\Delta R/R_0$) is less than $\pm 0.02\%$ (**Fig. S1**). This
143 tight adhesion and waterproof capability of the liquid bandage allow the strain sensor
144 working unaffectedly under large body movements and sweated skin surface. The
145 overall dimension of the strain sensor is 5 mm \times 2 mm (length \times width) and a 6.2 μm
146 of thickness, making it more convenient and comfortable as attached to the human
147 body, as shown in **Fig. 1c**. Compared with the recent reported piezoresistive strain
148 sensors, our device demonstrates superiorly tiny size with competitive stretching
149 range and sensitivity, shown in **Table S1**. The ultra-thin design combing with
150 filamentary fractal Au wires allows the device to be stretched, bent and twisted for
151 seamless and conformal integration onto curvilinear surfaces of human epidermis (**Fig.**
152 **1d** and **1e**). It is tested that most of the skin surface would stretch within 20%, without
153 any external stretching (Table S2). It indicates that the strain sensor could be mounted
154 on most of the body parts for the body movement monitoring. The finite element
155 analysis (FEA) shows that the maximum equivalent strain in Au is less than the yield
156 strain 0.3% for the device under 280° bending (bending radius \sim 2.7 mm), 20%

157 stretching, and 90° twisting (**Fig. 1d**). These results highlight the robust, and
 158 stretchable device which can operate under realistic physiological loads.

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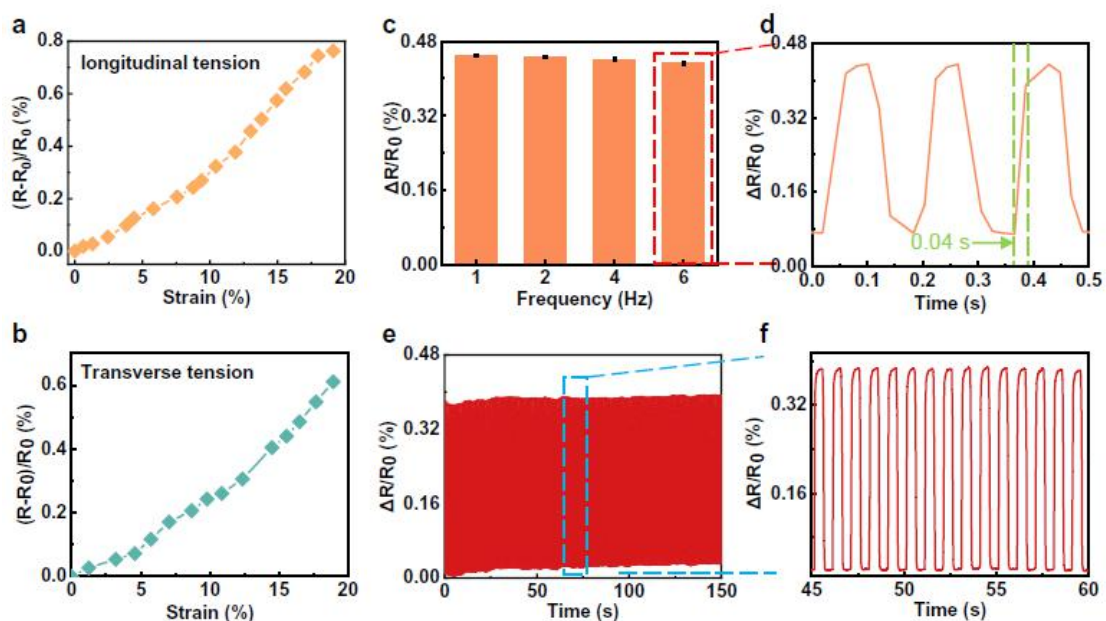
161 **Fig. 1.** Flexible, ultrathin, skin-integrated, and Au-based strain sensor. (a) Schematic
 162 diagram of the strain sensor. (b) The optical image of the patterned Au/Cr electrode
 163 design. (c) Optical image of the strain sensor mounted on the human epidermal
 164 surface. (d) FEA results of strain distribution on strain sensor under stretching,
 165 twisting, and bending. (e) Optical image of the strain sensor attached on a pink PDMS
 166 surface with three mechanical deformations, including bending, stretching, and
 167 twisting.

168

169

170 **Fig. 2a** and **2b** present the electrical signal ($\Delta R/R_0$) as a function of strain variation
 171 under the static state along length and width, respectively. It is obvious that the
 172 electrical response increases linearly with the increase of the strain along the two
 173 directions. At the strain change of 20%, the values of $\Delta R/R_0$ can reach to 0.76% and
 174 0.61% under longitudinal and transverse tensions, respectively. It is proved that the
 175 strain sensor is sensitive to both longitudinal and transverse strain and it is able to
 176 function at the 20% strain at either direction. To investigate the frequency effect on
 177 the electrical signal, the device was tested under a constant strain variation (12.5%)
 178 with different frequencies from 1 Hz to 6 Hz, fully covering the frequencies triggered
 179 by human daily motions, as shown in **Fig. 2c**. It is found that the low frequency has
 180 no effect on the electrical response of the device due to its fast response time (0.04 s)
 181 (**Fig. 2d**). To demonstrate the high durability of the strain sensor, fatigue tests were
 182 conducted with repeated stretching for 150 cycles at 1 Hz under 11.8% strain (**Fig. 2e**)
 183 with electrical signals ranging from 0% to 0.4% (**Fig. 2f**). The results prove that the
 184 strain sensor is tough enough to endure highly intensive stretching and maintain stable
 185 electrical signal outputs.

186



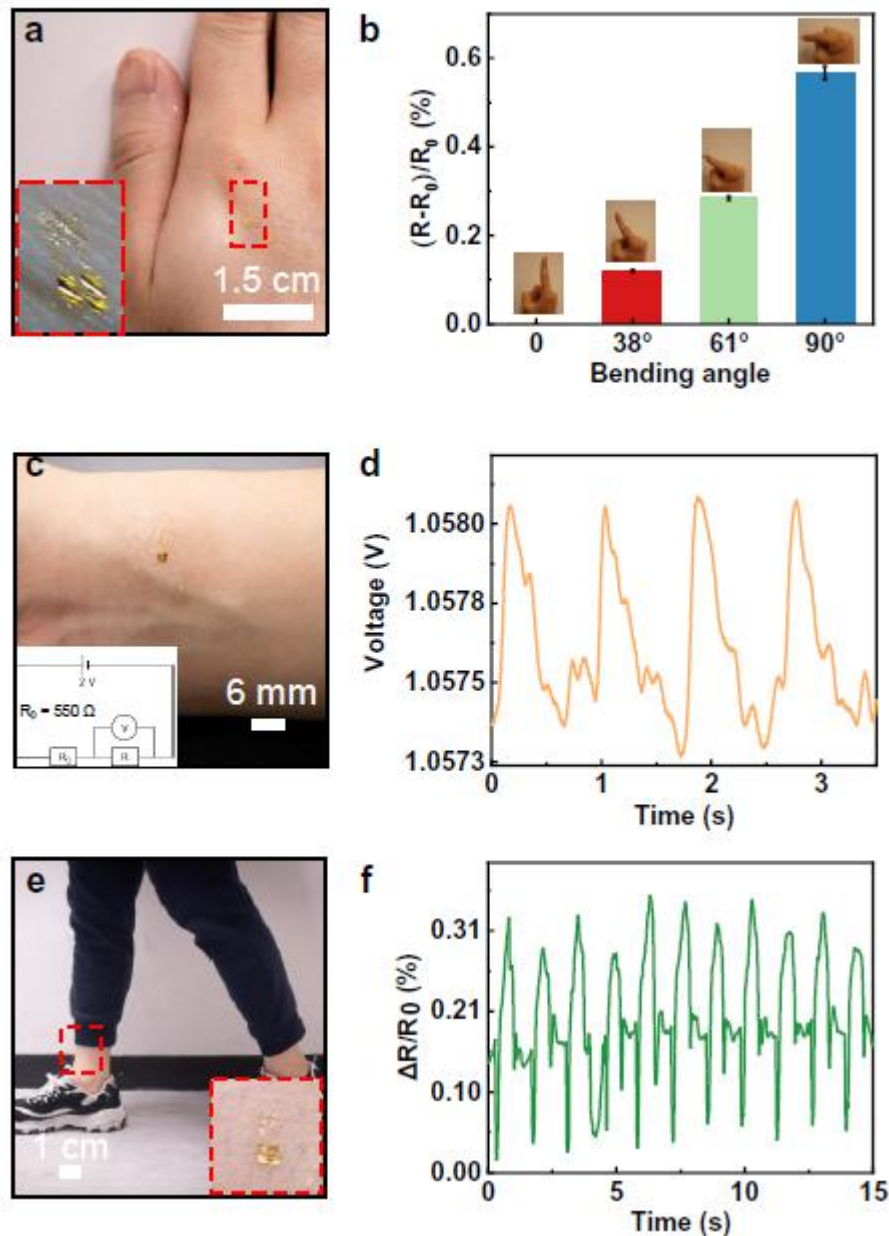
187

188 **Fig. 2.** The electrical characteristics of the strain sensor. **(a)** Electrical signals ($\Delta R/R_0$)
189 of the strain sensor at different longitudinal tensions. **(b)** Electrical signals ($\Delta R/R_0$)
190 of the strain sensor at different transverse tensions. **(c, d)** Electrical signals ($\Delta R/R_0$) of
191 the strain sensor at different frequencies under 12.5% strain and its detailed signals at
192 6Hz. **(e, f)** Electrical signals ($\Delta R/R_0$) of the strain sensor in a fatigue test for 150
193 cycles and its detailed signals from a selected range.

194

195 To further demonstrate its meticulous structure, the sensor is mounted on the back of
196 a hand (**Fig. 3a**). Due to its ultrathin thickness and good adhesion of the encapsulation
197 layer, the device can be conformally mounted onto human skin without any
198 delamination during stretching. As shown in **Fig. 3b**, the electrical signals ($\Delta R/R_0$) at
199 the bending angles of 38 °, 61 °, and 90 ° are 0.121%, 0.285%, and 0.567%
200 respectively. It proves that the strain sensor is capable of capturing small body
201 movements and output obvious signals, which are later applied in robotics control.
202 Shown in **Fig. 3c, d**, a sensor is attached onto an experimenter's wrist for pulse rate
203 recording (given with its circuit diagram), where the measured relative voltage shows
204 a regular variation ranging from 0% to 0.073%, along with the pulse rate. It is
205 sensitive towards the human pulse, which demonstrates the potential of the flexible
206 skin-integrated sensors in fields of clinical application. In **Fig. 3e**, it shows an optical
207 image of the strain sensor mounted on a volunteer's ankle for his walking motion
208 detection. The $\Delta R/R_0$ varies along with the paces, ranging from 0.0173% to 0.354%
209 (**Fig. 3f**), which shows its capability of human motion capturing. Its sensitivity toward
210 muscle contraction could be possibly applied in the field of motion detection in sports.

211



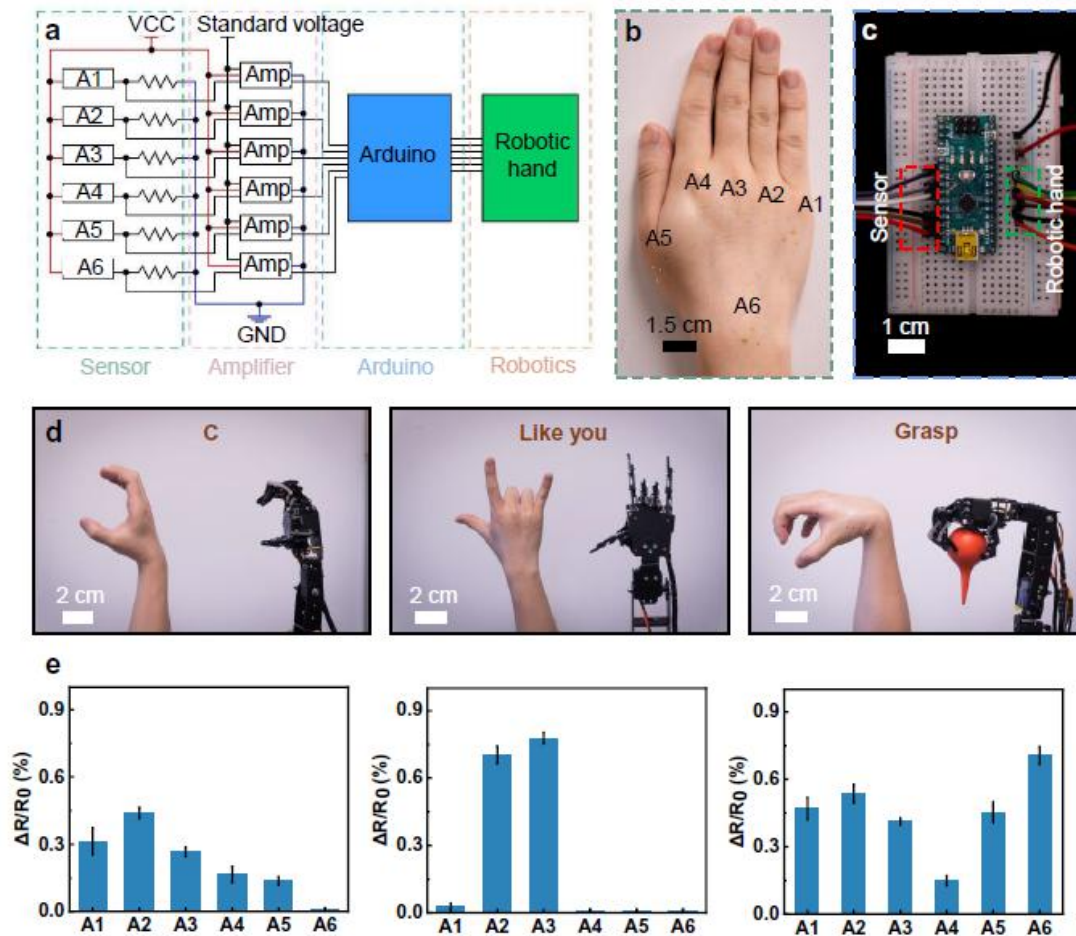
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213 **Fig. 3.** The electrical signals of the flexible strain sensor under different external
 214 stimuli. (a) Optical image of the strain sensor mounted on the back of a hand and its
 215 enlarged optical image of the strain sensor during deformation. (b) Electrical signals
 216 ($\Delta R/R_0$) of the strain sensor under different finger bending angles (c) Optical image of
 217 strain sensor mounted on a waist for human pulse rate detection and its electrical
 218 diagram (d) Electrical signals (Voltage) of the strain sensor in the pulse rate test in (c).
 219 (e) Optical image of strain sensor mounted on a waist for ankle for walking motion
 220 detection. (f) Electrical signals ($\Delta R/R_0$) of the strain sensor under the walking motion
 221 test.

222

223 Next, the strain sensor is applied for the human-machine interface by demonstrating
224 the robotic hand control. The schematic diagram of the testing circuit is shown in **Fig.**
225 **4a**, in which the control system is composed with six strain sensors and their
226 corresponding amplifiers (INA828, Texas Instrument), and an Arduino board. **Fig. 4b**,
227 and **c** show the optical images of the strain sensors mounted on the joints of a hand
228 and circuits connected with the Arduino board (Arduino nano with ATMEGA328P-
229 MU chip) respectively. Those sensors are mounted on the joints of the hand to capture
230 the finger motions, which lead to a smooth control of the robotic hand. It is able to
231 imitate the gestures of the hand almost without any detention. In **Fig. 4d**, some
232 meaningful hand gestures, including “C”, “Like you”, and “Grasp”, are demonstrated,
233 which proves the high feasibility of robotic hand control. Moreover, there are three
234 corresponding graphs underneath illustrating the electrical responses of the sensors at
235 different hand gestures. It demonstrates the signal intensity varies with the hand’s
236 bending degree that at the fingers’ complete bending and straightening conditions, the
237 electrical signals ($\Delta R/R_0$) are 0.75% and 0.04% respectively (**Fig. 4e**). This distinct
238 disparity of the electrical signals leads to the accurate control of the robotic hand. To
239 summarize, we demonstrated a human-machine interface application of the strain
240 sensor by controlling a robotic hand in a natural and smooth approach, there is high
241 feasibility of applying flexible strain sensors in application of human-machine
242 interface.

243



244

245 **Fig. 4.** Robotic hand controlling performed by the flexible strain sensors. (a) The
 246 schematic diagram of the testing circuit for controlling robotic hand. (b) Optical
 247 image of six sensors mounted on the joints of a hand for robotic hand control. (c)
 248 Optical image of the Arduino breadboard linked with the sensors and the robotic hand.
 249 (d) Optical image illustrating that the sensors control the robotic hand to make
 250 gestures of “C”, “like you” and “grasp” and their corresponding electrical signals
 251 ($\Delta R/R_0$) of the sensors at different gestures (e).

252

253

254 CONCLUSION

255 As a summary, an ultrathin Au-based stretchable strain sensor has been developed for
 256 body motions caption and human-machine interface. It owns advantages of
 257 miniaturized dimensions ($5 \text{ mm} \times 2 \text{ mm} \times 6.2 \mu\text{m}$), skin integrability, high stability,
 258 and stretchability which allow it to be tightly mounted on the epidermal surface for
 259 body motion capturing. Its electrical signal output $\Delta R/R_0$ can raise to 0.76% and

260 0.61% under 20% longitudinal and transverse stretching rate, respectively, and it can
261 undergo repeated stretching for 150 cycles at 1 Hz under 11.8 % strain. With liquid
262 bandage as the encapsulation, the strain sensor can be tightly mounted on epidermal
263 surface that can measure the human pulse rate and the walking motions. Furthermore,
264 the strain sensors are applied in robotic hand control, which can imitate the finger
265 motions of the human hand precisely, smoothly, and almost without any detention.
266 The results in this work present the potential in body motion measuring and robotic
267 control, which indicates a new strategy of the flexible sensors in the field of clinical
268 application and the human-machine interface.

269

270 **EXPERIMENTAL SECTION**

271 **Assembly of the tattoo-like electronic skin**

272 First, A quartz glass was cleaned with acetone, ethanol and deionized water (DI
273 water), sequentially. Then, PMMA solution (20mg/ml) was spin-coated onto the
274 surface of the cleaned glass at 2000 rpm for 30s, and then baked on the hotplate at 200
275 °C for 20 min. The PMMA thin film served as a sacrificial layer. Afterwards, poly-
276 amic acid solution (12.0 wt.% ± 0.5 wt.%, 3 μm) was spin-coated on the PMMA
277 sacrificial layer at 3000 rpm for 30s. Then, the PI thin film was cured on the hotplate
278 at 250 °C for 30 min to densify. Cr (40 nm) and Au (200 nm) were next deposited on
279 the PI film by magnetron sputtering, and then patterned with photolithography and
280 further wet etched to form the desired pattern. The photolithography process was
281 carried out by exposure the pre-spin-coated (3000 rpm, 30s) and soft baked (110 °C, 3
282 min) positive photoresist (PR, AZ 5214, AZ Electronic Materials) to the ultraviolet
283 light for 5 s. The pattern was then developed in AZ 300MIF developer for 15s and
284 followed with a post bake at 110 °C for 3 min. After etching the Au/Cr layer, the PR
285 was removed with acetone, and rinsed with DI water. A second layer of PI thin film (2
286 μm) was then spin coated (3000 rpm, 30s) and annealed (250 °C, 30 min), followed
287 by selectively dry etching (Oxford Plasma-Therm 790 RIE system, 200 W, 10 min).
288 The patterned PI thin film served as the encapsulation layer covering the whole
289 interconnects except the electrode areas. Next, the sample was immersed in acetone
290 for 12 h to fully dissolve the PMMA layer. Water soluble tapes (WSTs) were utilized
291 as a stamp to pick up the prepared pattern. Spray an ultrathin layer of liquid bandage
292 (1 μm, Banitore company) on the target area of human skin. Tightly attaching the

293 WSTs on the target area, then dried in the air at 25 °C for 5 min formed strong
294 mechanical bonding. Immersing the sample in water to remove the WSTs and realized
295 stretchable electrodes on human skin. Next, a liquid bandage layer (1 μm) was
296 sprayed on the top of the electrode. Dry the liquid bandage in the air for 5 min,
297 forming a robust structure with strong interface bonding between different layers.

298

299 **Characterizations**

300 The resistance was measured by a DAQ6510 data acquisition/multi-meter system.
301 The tiny voltage variance in **Fig. 3d** was calculated by measuring the voltage of a
302 fixed value resistor which connected in series with the triboelectric nanogenerator (the
303 voltage was measured by PL3516/P Powerlab 16/35, which owns much lower noise
304 signal and higher sampling rate than the DAQ6510 multimeter system).

305

306 **Mechanical simulation**

307 The finite element analysis commercial software ABAQUS (Analysis User's Manual
308 2016) was utilized to design the layout of strain sensor and study the corresponding
309 mechanical performance. The objective was to decrease the strain level in Au layer
310 under different typical loads (stretching, bending and twisting). The phantom skin was
311 modeled by hexahedron elements (C3D8R) while the thin Au, Cr, LB and PI layers
312 was modeled by shell elements (S4R). The minimal element size was 1/4th of the
313 width of the Au wires (50 μm), which ensured the convergence of the mesh, and the
314 accuracy of the simulation results. The elastic modulus (E) and Poisson's ratio (ν)
315 used in the analysis were $E_{Au}=78$ GPa, $\nu_{Au}=0.41$; $E_{PI}=2.5$ GPa, $\nu_{PI}=0.34$;
316 $E_{skin}=60$ kPa, $\nu_{skin}=0.5$; $E_{Gr}=294$ GPa, $\nu_{Gr}=0.21$ and $E_{LB}=85$ MPa, $\nu_{LB}=0.42$.

317

318 **DECLARATIONS**

319 **Author contributions**

320 Wrote and reviewed the manuscript: Wong T, Yiu C, Zhou J, Song Z, Liu Y, Zhao L,
321 Yao K, Park W, Yoo W, Song E, Xie Z, Yu X

322

323 **Availability of data and materials**

324 Not applicable.

325

326 **Financial support and sponsorship**

327 This work was supported by City University of Hong Kong (Grants No. 9610423,
328 9667199, 9667221, 9680322), Research Grants Council of the Hong Kong Special
329 Administrative Region (Grant No. 21210820, 11213721), Shenzhen Science and
330 Technology Innovation Commission (Grant No. JCYJ20200109110201713). Z.X.
331 acknowledges the support from the National Natural Science Foundation of China
332 (Grant No. 12072057), Liaoning Revitalization Talents Program (Grant No.
333 XLYC2007196), and Fundamental Research Funds for the Central Universities (Grant
334 No. DUT20RC(3)032). E.S. acknowledged the support from Shanghai Municipal
335 Science and Technology Major Project (No.2018SHZDZX01), ZJ Lab, and Shanghai
336 Center for Brain Science and Brain-Inspired Technology.

337

338 **Conflicts of interest**

339 All authors declared that there are no conflicts of interest.

340

341 **Consent for publication**

342 Not applicable.

343

344 **Ethical approval and consent to participate**

345 Not applicable.

346

347 **Consent for publication**

348 Not applicable.

349

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