

Review

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# Design of super-elastic freestanding ferroelectric thin films guided by phase-field simulations

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## Abstract

Understanding the dynamic behavior of domain structures is critical to the design and application of super-elastic freestanding ferroelectric thin films. Phase-field simulations represent a powerful tool for observing, exploring and revealing the domain-switching behavior and phase transitions in ferroelectric materials at the mesoscopic scale. This review summarizes the recent theoretical progress regarding phase-field methods in freestanding ferroelectric thin films and novel buckling-induced wrinkled and helical structures. Furthermore, the strong coupling relationship between strain and ferroelectric polarization in super-elastic ferroelectric nanostructures is confirmed and discussed, resulting in new design strategies for the strain engineering of freestanding ferroelectric thin film systems. Finally, to further promote the innovative development and application of freestanding ferroelectric thin film systems, this review provides a summary and outlook on the theoretical modeling of freestanding ferroelectric thin films.

**Keywords:** Freestanding ferroelectric thin films, super-elastic, mechanical structure, topological domain structure, phase-field simulations

## INTRODUCTION

The advancement of semiconductor materials and micro-/nanofabrication technologies has promoted the growth of the modern electronics industry. Various materials with excellent qualities which meet the needs



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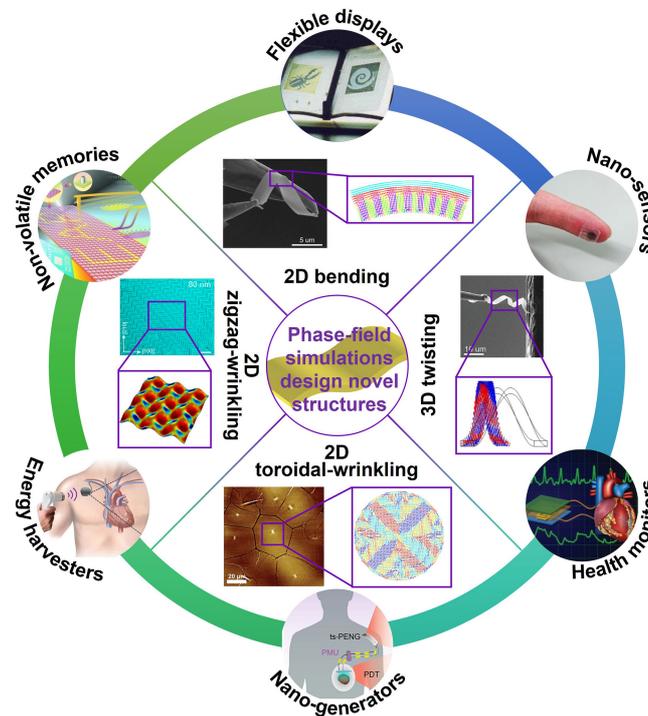


of the automated and intelligent manufacturing industries have been designed and prepared gradually. In recent decades, silicon-based complementary metal-oxide-semiconductor (CMOS)-centric design procedures have played a critical role in the modern electronics industry. However, the emergence of flexible electronic devices has presented new challenges for the traditional CMOS processing technique and new opportunities for the existing electronic manufacturing industry<sup>[1-3]</sup>. Flexible electronic materials can be applied to fabricate flexible displays<sup>[4-6]</sup>, nanosensors<sup>[7-9]</sup>, health monitors<sup>[10-12]</sup> and other electronic devices for intelligent processing and human-computer interactions<sup>[13]</sup>. For example, flexible electronic materials can integrate cutting-edge technologies, including intelligent signal processing, real-time information sensing and nanogenerators, to improve the intelligence level of biocompatible electronics. As a result, they play an increasingly critical role in the intelligent monitoring of human health and biomedical applications, which will significantly change the future of healthcare and the relationship between patients and electronics. Furthermore, with the rise and combination of artificial intelligence and the Internet of Things (AI and IoT, i.e., AIoT), these electronic devices have an increasingly wide range of applications.

However, most traditional inorganic materials with excellent electronic properties show poor stability in complex stress environments, thereby severely limiting their application prospects in flexible electronic devices. Therefore, finding and preparing basic materials with excellent electronic and flexible properties is one of the keys to developing the flexible electronics industry. Generally, two complementary approaches can be applied to obtain electronic materials with superior mechanical and electrical properties. The first is the design and innovation of flexible materials by developing novel materials, including polymers<sup>[14,15]</sup>, hydrogels<sup>[16,17]</sup>, liquid metals<sup>[18,19]</sup> and freestanding films<sup>[20,21]</sup>. The second is structural optimization design by designing traditional high-performance electronic materials into appropriate mechanical structures<sup>[22,23]</sup>, including wrinkled<sup>[24,25]</sup>, origami<sup>[26,27]</sup>, kirigami<sup>[28,29]</sup> and textile<sup>[30,31]</sup> structures.

Ferroelectric perovskite oxides are indispensable materials in the modern electronics industry because of their abundance of excellent physical properties, extensive research value and long-term practical application prospects. High-performance ferroelectric oxides are critical components in the current electronics industry because they have outstanding electrical properties, including ferroelectricity, piezoelectricity, pyroelectricity and dielectricity. They are widely applied in high-efficiency memories<sup>[32-35]</sup>, microsensors<sup>[36,37]</sup>, high-frequency filters<sup>[38,39]</sup>, energy harvesting systems<sup>[40,41]</sup>, high-energy-density capacitors<sup>[42-45]</sup>, ultrasonic medical treatment<sup>[46,47]</sup> and other related devices<sup>[48-51]</sup>, and are also expected to be applied in the field of high-temperature superconductivity<sup>[52,53]</sup>. However, perovskite ferroelectrics are generally considered to be brittle and unbendable<sup>[54,55]</sup>. Therefore, if they can be transformed into flexible structures through the above two approaches, it will significantly accelerate the growth of the flexible electronics industry and occupy increasingly widespread applications. In addition, organic ferroelectric polymer materials<sup>[56-60]</sup>, such as poly(vinylidene fluoride) and its copolymers, have excellent properties and can achieve sizeable mechanical deformation, such as stretching, bending and twisting, without being damaged. Therefore, for the design and processing of flexible electronic materials, ferroelectric materials with flexibility and super-elasticity have received extensive attention due to their excellent mechanical and electrical properties.

This review mainly focuses on super-elastic freestanding ferroelectric thin films. First, current super-elastic freestanding ferroelectric films and their experimental characterization results are summarized. Subsequently, the origin of the super-elasticity of freestanding ferroelectric thin films is revealed and explained on the basis of phase-field simulations. The designed mechanical structures based on super-elastic ferroelectric thin films, such as two-dimensional (2D) wrinkles and three-dimensional (3D) nanosprings, are then introduced [Figure 1]. Finally, the outlook and prospects for super-elastic flexible freestanding



**Figure 1.** Novel mechanical structures and applications of super-elastic/flexible freestanding ferroelectric thin films. Novel mechanical structures include 2D bending (Left : reprinted with permission<sup>[61]</sup>. Copyright 2019, The American Association for the Advancement of Science. Right: reprinted with permission<sup>[62]</sup>. Copyright 2020, AIP Publishing), 2D zigzag-wrinkling (Top: reprinted with permission<sup>[63]</sup>. Copyright 2020, Wiley-VCH. Bottom: reprinted with permission<sup>[64]</sup>. Copyright 2022, American Chemical Society), 2D toroidal-wrinkling (reprinted with permission<sup>[65]</sup>. Copyright 2021, The American Association for the Advancement of Science), and 3D twisting (reprinted with permission<sup>[66]</sup>. Copyright 2022, Wiley-VCH) structures. Flexible applications include non-volatile memories (reprinted with permission<sup>[67]</sup>. Copyright 2013, Wiley-VCH), flexible displays (reprinted with permission<sup>[68]</sup>. Copyright 2004, Elsevier), nano-sensors (reprinted with permission<sup>[69]</sup>. 2018, CC BY license), health monitors (reprinted with permission<sup>[70]</sup>. Copyright 2016, Wiley-VCH), nano-generators (reprinted with permission<sup>[71]</sup>. Copyright 2020, American Chemical Society), and energy harvesters (reprinted with permission<sup>[72]</sup>. 2016, CC BY license).

ferroelectric thin films are presented.

## SUPER-ELASTIC FREESTANDING FERROELECTRIC FILMS

### Preparation of flexible ferroelectric thin films

Due to the clamping effect of the rigid substrates during the traditional process of preparing ferroelectric thin films, they often show far poorer electrical performance, in terms of piezoelectric constant, switching speed and switching voltage<sup>[73-76]</sup>, than those of freestanding materials. With the rapid development of new fabrication techniques for thin films<sup>[77]</sup>, high-quality flexible freestanding ferroelectric thin films with excellent mechanical elastic and electrical properties<sup>[78,79]</sup> can be fabricated. Since many excellent reviews<sup>[21,80-83]</sup> have discussed the preparation of flexible freestanding ferroelectric films, we only briefly summarize the methods for obtaining them here.

**Direct growth.** Ferroelectric thin films can be directly grown on flexible substrates, including metals (such as foils), organic polymers (such as polyimide (PI)) and 2D layered materials (such as mica and graphene). Metal foils have low brittleness, excellent electrical conductivity and outstanding thermal stability as flexible substrates. Due to the unfavorable thermal expansion mismatch and ion diffusion between the ferroelectric thin film and the metal foil, a buffer layer is usually grown on the surface of the substrate to solve these problems. For instance, Won *et al.* used  $\text{LaNiO}_3$ , which has closely matched lattice parameters ( $\sim 0.38$  nm)

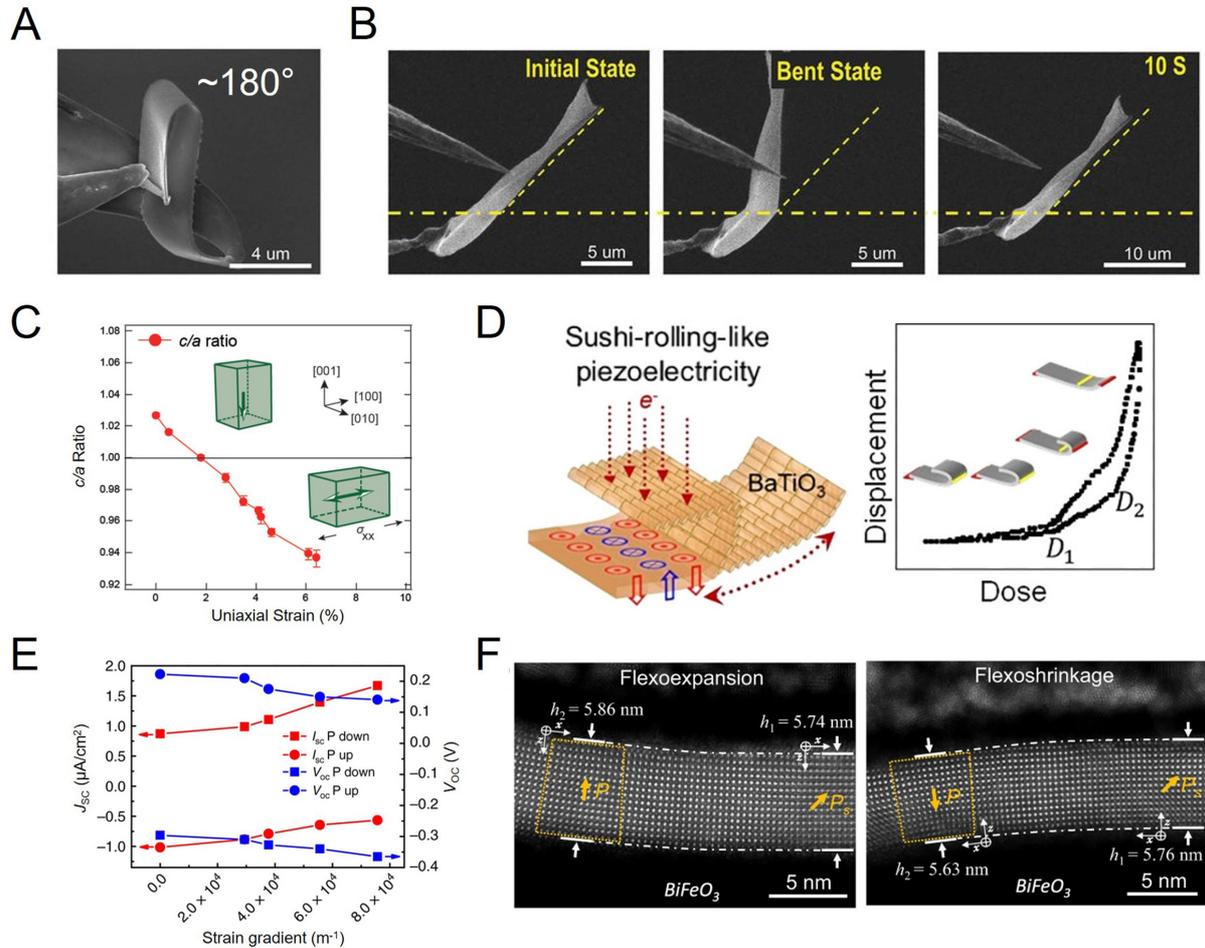
with most perovskite ferroelectric materials, as a conductive buffer layer and the prepared  $\text{Pb}(\text{Zr,Ti})\text{O}_3$  films exhibited superior ferroelectricity and piezoelectricity than those on conventional  $\text{Pt/Ti/SiO}_2/\text{Si}$  substrates<sup>[84]</sup>. Although PI substrates have better mechanical ductility and flexibility, the temperature they can withstand ( $< 400^\circ\text{C}$ ) cannot reach the crystallization temperature of ferroelectric oxides ( $> 600^\circ\text{C}$ ). Bretos *et al.* proposed a series of solution-based approaches to realize the low-temperature crystallization of ferroelectric thin films, such as  $\text{BiFeO}_3$  and  $\text{Pb}(\text{Zr,Ti})\text{O}_3$ <sup>[85-89]</sup>. In addition to the aforementioned direct growth on flexible substrates, mechanical exfoliation along heterointerfaces after the deposition of ferroelectric thin films onto 2D layered materials has also been developed. Through van der Waals epitaxy, weak bonds are formed between the thin film and the 2D layered substrate, providing an opportunity for mechanical exfoliation to obtain freestanding ferroelectric thin films with minimal internal stress. Mica<sup>[90-92]</sup> and graphene<sup>[93,94]</sup> are promising 2D layered materials as flexible substrates with atomic-level surface roughness, good stability and mechanical flexibility. High-quality flexible ferroelectric films with good mechanical integrity can be grown on mica and graphene substrates by van der Waals epitaxy, demonstrating their potential for next-generation electronics.

**Laser lift-off process.** The laser lift-off method was initially proposed and developed for transferring epitaxial GaN films from substrates<sup>[95,96]</sup> and was later utilized to prepare and obtain flexible freestanding ferroelectric oxide films. The specific process is to first deposit a ferroelectric oxide film (such as via a sol-gel method) on a wide band gap substrate (such as sapphire). A laser then irradiates the sample from the back of the substrate to partially vaporize the interface between the ferroelectric film and the substrate. Finally, a freestanding ferroelectric oxide film is obtained. However, this stripping method ablates the ferroelectric thin film, forming a thermally damaged layer at the interface of the thin film, so it is necessary to introduce a sacrificial layer<sup>[97,98]</sup> and further anneal to recover the surface structure<sup>[99]</sup>.

**Wet etching.** Obtaining freestanding ferroelectric thin films by wet etching is a promising approach with significant advantages. According to the parts to be etched, wet etching can be divided into wet etching of the substrate, wet etching of the interface layer between the thin film and substrate and wet etching of the sacrificial layer, with the latter being the more cost-effective method<sup>[99]</sup>. Single-crystal ferroelectric thin films have been grown on sacrificial buffer layer (e.g.,  $\text{La}_{0.7}\text{Sr}_{0.3}\text{MnO}_3$ <sup>[100,101]</sup>,  $\text{Sr}_3\text{Al}_2\text{O}_6$ <sup>[102-106]</sup> and  $\text{BaO}$ <sup>[107]</sup>)-coated  $\text{SrTiO}_3$  (STO) substrates. Subsequently, the sacrificial buffer layer is dissolved by selective etching to release the freestanding ferroelectric oxide film. Finally, the freestanding thin films can be transferred to flexible substrates, such as polyethylene terephthalate<sup>[75,108]</sup> or polydimethylsiloxane (PDMS)<sup>[61,105,109-111]</sup>. They can also be transferred to silicon (Si) substrates and combined with Si-based electronics. For example, Han *et al.* selected water-soluble  $\text{Sr}_3\text{Al}_2\text{O}_6$  as the sacrificial layer to grow a series of  $(\text{PbTiO}_3)_m/(\text{SrTiO}_3)_n$  bilayers on STO substrates. After the  $\text{Sr}_3\text{Al}_2\text{O}_6$  sacrificial layer was dissolved, the bilayer films were laminated on a platinized Si (001) substrate<sup>[112]</sup>. Exotic skyrmion-like polar nanodomains are observed in bilayer films, which provide a new strategy for integration into Si-based high-density storage technologies.

### Super-elastic behavior of freestanding single-crystal ferroelectric thin films

Ferroelectric oxides are generally considered to be brittle and non-bendable because of their grain boundaries and the small ductility of ionic or covalent bonds within the crystal. In addition, the low fracture toughness (in the order of  $1 \text{ MPa}\cdot\text{m}^{1/2}$ )<sup>[55]</sup> means that ferroelectric oxides are prone to fracture. Nevertheless, the high-quality freestanding single-crystal ferroelectric thin films obtained by the above freestanding methods have attractive mechanical flexibility and super-elasticity. Dong *et al.* fabricated freestanding single-crystal  $\text{BaTiO}_3$  (BTO)<sup>[61]</sup> and  $\text{BiFeO}_3$  (BFO)<sup>[110]</sup> ferroelectric thin films by pulsed-laser deposition (PLD) when using  $\text{Sr}_3\text{Al}_2\text{O}_6$  as a sacrificial layer that was dissolved in water. As shown in [Figure 2A](#) and [B](#), the fabricated BTO films could undergo a  $\sim 180^\circ$  folding without any cracks in in-situ scanning electron microscopy (SEM) bending tests and also recover to their original shape after removing the bending load.



**Figure 2.** (A) In situ SEM image of the BTO film folded to about 180°. (B) SEM images of bending and recovery process of a BTO film. (C) The  $c/a$  ratio of freestanding PTO films as a function of uniaxial strain. The inset is schematics of as-grown and stretched polarization state. (D) Electromechanical coupling responses of freestanding BTO films folded and unfolded under an electron beam-induced field. (E) Open circuit voltage ( $V_{oc}$ ) and short circuit current density ( $J_{sc}$ ) of freestanding BFO device as a function of strain gradient. (F) The bending-expansion and bending-shrinkage effects were observed in upward and downward bent BFO films. Panels A and B reprinted with permission<sup>[61]</sup>. Copyright 2019, The American Association for the Advancement of Science. Panel C reprinted with permission<sup>[106]</sup>. Copyright 2020, Wiley-VCH. Panel D reprinted with permission<sup>[113]</sup>. Copyright 2020, American Chemical Society. Panel E reprinted with permission<sup>[109]</sup>, 2020, CC BY license. Panel F reprinted with permission<sup>[114]</sup>, 2022, CC BY license.

This behavior demonstrates their super-elasticity and flexibility. Similarly, the BFO film could withstand cyclic folding tests of up to 180° and the largest bending strain was observed to reach 5.42% during the bending process. Furthermore, freestanding flexible multiferroic BiMnO<sub>3</sub> films were synthesized by Jin *et al.*, which could maintain mechanical integrity under nearly 180° folding<sup>[111]</sup>.

Freestanding thin films, in contrast to epitaxial thin films, are free from the clamp of the substrate and therefore provide ideal and unique flexible platforms for continuously controllable strain engineering. For example, Han *et al.* applied a continuous uniaxial tensile strain as high as 6.4% to freestanding PbTiO<sub>3</sub> (PTO) films, far exceeding the realizable value for epitaxial PTO films [Figure 2C]<sup>[106]</sup>. This demonstrates the efficient and meaningful strain tunability of freestanding ferroelectric films, which deserves further exploration and design. Flexible freestanding oxides also provide a new direction for exploring outstanding performance, including piezoelectricity and flexoelectricity. By PLD, Elangovan *et al.* fabricated 30-nm-thick flexible freestanding piezoelectric BTO thin films with good electromechanical-coupling

properties<sup>[113]</sup>. As shown in **Figure 2D**, under an external electric field, the thin film could fold gradually and continuously by 180° and the fold-unfold cycles were reversible. The contribution of the flexoelectric effect caused by the strain gradient induced by bending in flexible films is considerable. Guo *et al.* demonstrated the tunable photovoltaic effect in freestanding single-crystal BFO films and obtained multilevel photoconductance in BFO by altering the bending radius of the flexible device [**Figure 2E**]<sup>[109]</sup>. As shown in **Figure 2F**, Cai *et al.* observed a giant flexoelectric response at strain gradients of up to  $\sim 3.5 \times 10^7 \text{ m}^{-1}$  in a wrinkled structure based on high-quality flexible freestanding BFO perovskite oxides<sup>[105,114]</sup>. Furthermore, the unusual bending expansion and shrinkage observed in bent freestanding BFO are also never seen in crystalline materials. Corresponding theoretical models show that these novel phenomena are attributed to the combined action of flexoelectricity and piezoelectricity. These experimental observations and theoretical models may provide a new path toward the strain and strain-gradient engineering of super-elastic freestanding ferroelectric thin films.

## PHASE-FIELD METHOD OF FERROELECTRICS

The mechanical, electrical, optical, magnetic and other macroscopic physical properties of a material are not only related to its chemical composition but also largely depend on the characteristics of its internal microstructure. Such microstructures can be phase structures composed of crystalline structures, grains with different orientations, ferroelectric domains and dislocations, which are usually at the mesoscopic scale, ranging from nanometers to micrometers<sup>[115]</sup>. In material processing and service, external stimuli may cause the microstructure to move away from equilibrium. Furthermore, the corresponding theoretical description requires a combination of non-equilibrium thermodynamics and kinetic theories. Thermodynamic theory and kinetic principles determine the evolution direction and path of the microstructure, respectively. Due to the complexity and nonlinearity of microstructural evolution, we usually use numerical simulation methods to predict the evolution process. Compared to traditional modeling methods involving the explicit tracking of interface locations, the phase-field method has become one of the most powerful methods for simulating the evolution process of various microstructures. The phase-field method is based on the Landau theory of phase transitions, which holds that one of the standard features of a phase transition is a change in the symmetry of a system. Changes in symmetry imply changes in the degree of order, which can be measured by the order parameter (as a space function). According to the selection of order parameters, ferroelectrics are classified as proper or improper. For BTO, PTO and other proper ferroelectrics, the selected order parameter is the ferroelectric polarization  $P$  that can explain the symmetry change in the phase transition. However, for improper ferroelectrics, such as hexagonal manganites  $h\text{-REMnO}_3$  (RE = rare earth), the primary order parameter is the amplitude  $Q$  and phase  $\Phi$  characterizing the structural trimerization and the secondary order parameter is the polarization  $P$  induced by the trimerization<sup>[116,117]</sup>.

### Theoretical fundamentals of phase-field method

The phase-field method with diffusive interfaces considers the non-local energy of the polarization gradient, which is different from the homogeneous assumption in thermodynamic models. By solving the phase-field equations, the order parameters in the space and time distribution can be calculated, the spatially continuous but inhomogeneous polarization distribution in the ferroelectric at different times can be determined and the evolution process of the microstructure can be obtained. The evolution process is a direct consequence of the minimization of the total free energy of the entire system, where ferroelectric polarization switching and phase transitions can be simulated by solving the time-dependent Ginzburg-Landau equation<sup>[118-122]</sup>:

$$\frac{\partial P_i(\mathbf{r}, t)}{\partial t} = -L \frac{\delta F}{\delta P_i(\mathbf{r}, t)}, i = x, y, z, \tag{1}$$

where  $P_i(\mathbf{r}, t)$  is the spontaneous polarization,  $\mathbf{r}$  is the spatial coordinate,  $t$  is the evolution time,  $L$  is the kinetic coefficient that is related to the domain evolution and  $F$  is the total free energy that includes the contributions from the Landau, gradient, elastic, electric and flexoelectric coupling energies:

$$F = \iiint_V [f_{Land}(P_i) + f_{grad}(P_{i,j}) + f_{elec}(P_i, E_i) + f_{elas}(P_i, \varepsilon_{ij}) + f_{flexo}(P_i, \varepsilon_{ij}, P_{i,j}, \varepsilon_{kl,j})] dV. \tag{2}$$

The Landau energy density  $f_{Land}$  and the gradient energy density  $f_{grad}$  are given by:

$$f_{Land} = \alpha_{ij} P_i P_j + \alpha_{ijkl} P_i P_j P_k P_l + \alpha_{ijklmn} P_i P_j P_k P_l P_m P_n, \tag{3}$$

$$f_{grad} = \frac{1}{2} G_{ijkl} P_{i,j} P_{k,l}, \tag{4}$$

where  $\alpha_{ij}$ ,  $\alpha_{ijkl}$  and  $\alpha_{ijklmn}$  are the Landau coefficients,  $G_{ijkl}$  is the gradient energy coefficient and  $P_{i,j} = \partial P_i / \partial x_j$ .

The electric energy density  $f_{elec}$  is expressed as:

$$f_{elec} = -E_i (P_i + \frac{1}{2} \varepsilon_0 \kappa_{ij} E_j), \tag{5}$$

where  $E_i$  is the electric field component,  $\varepsilon_0$  is the vacuum permittivity and  $\kappa_{ij}$  is the dielectric constant. The electrical quantities should satisfy the electrostatic equilibrium (Poisson's) equation:

$$-\nabla^2 \varphi = \frac{\rho - \nabla \cdot P_i}{\varepsilon_0 \kappa_{ij}}, \tag{6}$$

where  $\varphi$  is the electric potential and  $\rho$  represents the total space charges. The electric field is related to the potential through  $E_i = -\varphi_{,i}$ .

The elastic energy density  $f_{elas}$  and the flexoelectric coupling energy density  $f_{flexo}$  can be written as:

$$f_{elas} = \frac{1}{2} C_{ijkl} e_{ij} e_{kl} = \frac{1}{2} C_{ijkl} (\varepsilon_{ij} - \varepsilon_{ij}^0)(\varepsilon_{kl} - \varepsilon_{kl}^0), \tag{7}$$

$$f_{flexo} = -\frac{1}{2} f_{ijkl} (\varepsilon_{ij,i} P_k - \varepsilon_{ij} P_{k,i}), \tag{8}$$

where  $C_{ijkl}$  is the elastic stiffness tensor,  $e_{ij}$  is the elastic strain and  $\varepsilon_{ij}$  and  $\varepsilon_{ij}^0$  are the total local strain and eigenstrain, respectively. Moreover,  $\varepsilon_{ij}^0 = Q_{ijkl} P_k P_l$ , where  $Q_{ijkl}$  represents the electrostrictive coefficients.  $f_{ijkl}$  is the flexoelectricity tensor and there are three independent flexoelectric coupling coefficients for a material of cubic point group, namely, the longitudinal coupling coefficient  $f_{1111}$ , the transversal coupling coefficient  $f_{1122}$  and the shear coupling coefficient  $f_{1212}$ .

The mechanical quantities are satisfied by solving the mechanical equilibrium equation:

$$\sigma_{ji,j} + b_i = 0, \quad (9)$$

where  $\sigma_{ij}$  is the stress tensor and  $b_i$  is the external force per unit volume.

### Phase-field model of freestanding ferroelectric thin films

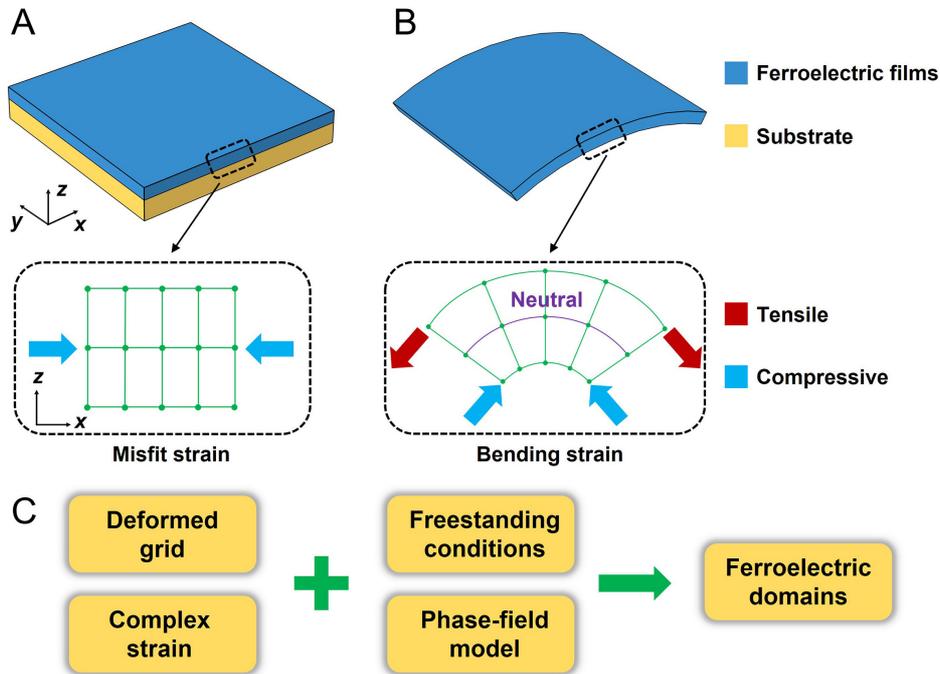
The phase-field model of a freestanding ferroelectric thin film differs from that of an epitaxial ferroelectric thin film with a substrate. As shown in [Figure 3A](#) and [B](#), the lattice points of traditional epitaxial ferroelectric thin film models are subjected to compressive (or tensile) misfit strains induced by the substrate. The lattice points in the new phase-field model of the freestanding ferroelectric thin film have deformability characteristics, which can change the volume and shape following the bending deformation of the thin film.

The deformation of freestanding ferroelectric films can be set by applying displacement or stress (strain) boundary conditions. For instance, Guo *et al.* achieved the bending deformation of a freestanding film by applying displacement boundary conditions, explicitly adjusting the rotational inclination of the left and right end of the film along the neutral surface<sup>[62]</sup>. Moreover, Peng *et al.* stabilized the film to a bending state by applying stress (strain) boundary conditions, explicitly introducing a bending strain state that exhibits a gradient distribution along the film thickness<sup>[110,123,124]</sup>. In addition, the top and bottom layers of the film are set as stress-free boundaries to satisfy the freestanding boundary conditions. Therefore, as shown in [Figure 3C](#), for the phase-field method of freestanding ferroelectric thin films, by using the well-established phase-field model of deformable lattices, considering the freestanding boundary conditions and the complex strain (and strain gradient) states caused by the deformation of novel mechanical structures, the nanodomains corresponding to the freestanding ferroelectric structure can be obtained. The mechano-electric coupling relationship and electrical properties (including piezoelectricity and electrocaloric performance) of the freestanding ferroelectric system can then be explored.

## MODEL-GUIDED UNDERSTANDING OF SUPER-ELASTICITY IN FREESTANDING FERROELECTRIC THIN FILMS

Freestanding thin films demonstrate the advantages of tunable strain states compared with epitaxial growth on lattice-mismatched substrates. The source of the superior super-elasticity of freestanding films needs to be further explored because it is crucial for their further application in flexible electronics. The super-elasticity of freestanding ferroelectric membranes may originate from the mesoscale ferroelectric domain evolution in the presence of the external deformation. However, the direct observation of the domain structure evolution of nanoscale freestanding films during continuous deformation is challenging by current experimental methods.

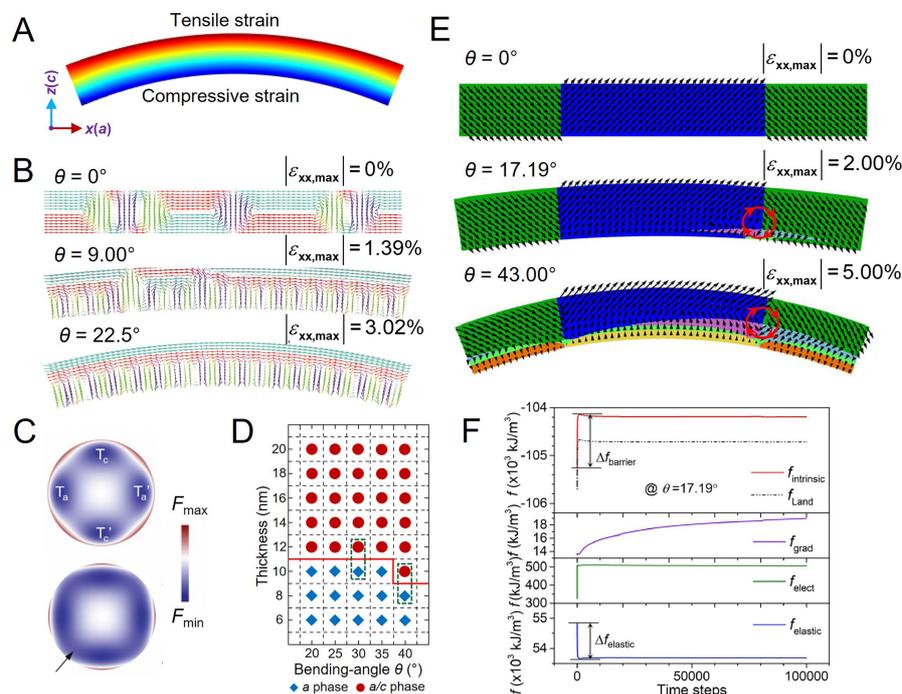
The phase-field method can simulate the dynamic evolution of freestanding ferroelectric films during mechanical deformation under external loads and the ferroelectric phase transition behavior under various strains and temperatures. Unlike the domain structure of ferroelectric films under a single strain in previous studies, more complex nanodomains appear due to the coexistence of tensile and compressive strains in bent freestanding films. For instance, Guo *et al.* and Peng *et al.* performed phase-field simulations on the bending deformation process of freestanding ferroelectric films to reveal the theoretical origin of the super-elasticity of freestanding ferroelectric films from the perspective of domain evolution<sup>[62,123]</sup>. During the continuous bending process of a freestanding BTO film, the mixed tensile and compressive stress generated



**Figure 3.** (A) Phase-field model of the epitaxial ferroelectric thin film with a substrate. The dashed box is a schematic of the model lattice under compressive misfit strain. (B) Phase-field model of the bent freestanding ferroelectric thin film. The dashed box is a schematic of the deformable model lattice under bending strain, and the purple line represents the neutral layer of the model. (C) The structural schematic of the phase-field method for freestanding ferroelectric thin films.

by the bending [Figure 4A] caused the electric dipole to rotate continuously in the transition region, thereby connecting the *a* and *c* domains to form “vortex-like” domain structures [Figure 4B]. The formation of “vortex-like” domains essentially eliminates the sharp stress caused by lattice mismatch, allowing the freestanding film to maintain mechanical integrity during the bending process. The continuous rotation of the electric dipole can be explained by the phenomenological Landau theory<sup>[61]</sup>. As seen from Figure 4C, four minima in the energy landscape exist in a bulk stress-free state of BTO, corresponding to two *a* domains and two *c* domains. When in the bending state, the energy barrier between the *a* and *c* domains decreases, indicating that the polarization transition between the *a* and *c* domains becomes easier. The appearance of “vortex-like” domains has apparent size effects and the *a/c* phase with a vortex-like structure emerges when the film thickness reaches 12 nm [Figure 4D]. This may indicate that the super-elasticity of freestanding ferroelectric films has a specific relationship with the film thickness.

From the perspective of phase-field energy minimization, the generation of a local ferroelectric vortex and the ferroelectric polarization rotation can effectively promote the reduction in elastic energy and modulate the mechanical stress on the freestanding ferroelectric film during bending, which contributes to the accommodation of the large deformation and super-elasticity. As shown in Figure 4E, Peng *et al.* investigated the dynamic domain evolution process of bent freestanding BFO films, with an exotic ferroelectric vortex generated by local ferroelastic switching when the bending angle was higher than the critical value (e.g., 17.19° for a thickness of 80 nm)<sup>[123]</sup>. By comparing the dynamic evolution of different energy densities during the phase-field simulation [Figure 4F], the intrinsic energy barrier ( $\Delta f_{\text{barrier}} = 1076.19 \text{ kJ/m}^3$ ) is overcome by reducing the elastic energy ( $\Delta f_{\text{elastic}} = 1157.65 \text{ kJ/m}^3$ ) when vortex domains are generated, which indicates that the minimization of elastic energy drives the generation of the vortex. As reviewed above from the perspective of domain structure evolution, the excellent mechanical

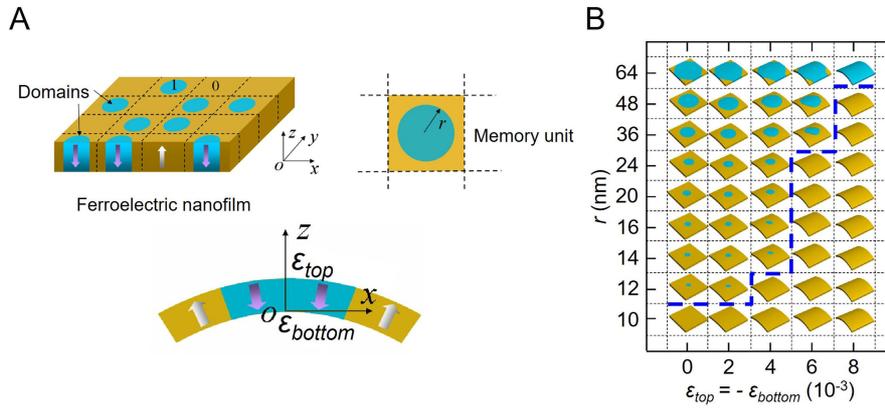


**Figure 4.** (A) Strain distribution of *n*-shape bent freestanding films. (B) Domain structures and surface strain of freestanding BTO thin film at different bending angles. (C) Schematic illustration of free energy landscape of bulk BTO (top) and freestanding thin films upon bending (bottom). (D) Size effect on domain patterns of BTO thin film under bending. (E) Dynamic evolution of ferroelectric domains in freestanding BFO thin films during bending. (F) Dynamic evolution of volume average energy density of freestanding BFO thin films under  $\theta = 17.19^\circ$  with time step. Panels A, B and D reprinted with permission. Copyright 2020, AIP Publishing<sup>[62]</sup>. Panel C reprinted with permission. Copyright 2019, American Association for the Advancement of Science<sup>[61]</sup>. Panels E and F reprinted with permission. Copyright 2021, Elsevier<sup>[123]</sup>.

elasticity of freestanding ferroelectric films can be attributed to the strong coupling effects between the bending strain state and electric dipoles, including the continuous rotation of polarization, the emergence of polar vortex domains and ferroelectric phase transitions.

## FUNCTIONAL MECHANICAL STRUCTURES BASED ON SUPER-ELASTIC FERROELECTRIC THIN FILMS

Freestanding ferroelectric thin films are ideal for studying the distortion of crystal structures and future applications of ferroelectric materials. Taking flexible carriers for memory logic devices as an example, Chen *et al.* systematically investigated the stability of  $180^\circ$  cylindrical domains in bent freestanding ferroelectric nanofilms and explored the possibility of mechanical erasure of bit information (“0” and “1”)<sup>[125]</sup>. Ferroelectrics are potential candidates for data storage due to their switchable spontaneous polarization. Figure 5A shows a freestanding PTO thin film divided into rectangular memory units, where the bit information “1” is represented by a cylindrical domain with downward polarization of radius  $r$ . From the phase diagram in Figure 5B, the bending deformation can effectively control the stability of the cylindrical domain and regulate the erasing of bit information. By changing the strain state of freestanding ferroelectric thin films, cylindrical domains can be erased, thereby providing a new theoretical idea for flexible memory devices. In addition to bending structures based on super-elastic freestanding ferroelectric films, other mechanical structures, such as 2D wrinkled and 3D nanospring structures, are also paving the way for novel flexible electronics.



**Figure 5.** (A) Schematic illustration of a ferroelectric nanofilm with rectangular memory units (upper left), a single basic memory unit (upper right), and a bent single memory unit (bottom). (B) Phase diagram of the domain pattern in memory units under bending. All panels reprinted with permission<sup>[125]</sup>, 2014, CC BY license.

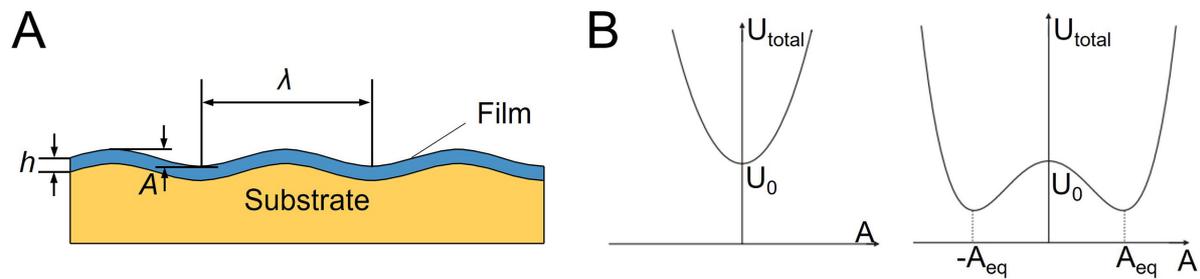
### 2D wrinkled structure of freestanding ferroelectric thin films

The buckling instability mode, which leads to out-of-plane deformation, is prone to occur in thin film structures under certain environmental stimuli (e.g., mechanical forces<sup>[126-130]</sup>, temperature<sup>[131]</sup>, van der Waals interactions<sup>[132]</sup> and localized diffusion of the solvent<sup>[133,134]</sup>). For example, when the film is subjected to in-plane compressive stress, it is in an unstable state with high energy. As a result, the film and substrate deform to release compressive stress, thereby reducing the energy of the system. Moreover, because the film thickness  $h$  is small, its bending rigidity  $D = E_f h^3/12$  is minimal compared to Young's modulus  $E_f$ . Films generally deform via out-of-plane wrinkling to release internal compressive stress by generating bending energy. For the simplest sinusoidal wrinkling mode  $w(x,y) = A \cos(kx)$ , both the wavelength and amplitude are related to the mechanical quantities of the film-substrate system<sup>[135-139]</sup>:

$$\begin{aligned} \lambda &= 2\pi h \left( \frac{\bar{E}_f}{3\bar{E}_s} \right)^{\frac{1}{3}}, \\ \varepsilon_c &= \frac{1}{4} \left( \frac{3\bar{E}_s}{\bar{E}_f} \right)^{\frac{2}{3}}, \\ A &= h \left( \frac{\varepsilon}{\varepsilon_c} - 1 \right)^{\frac{1}{2}}, \\ \bar{E} &= \frac{E}{1-\nu^2}, \end{aligned} \tag{10}$$

where  $E_f$  and  $E_s$  are Young's modulus of the film and substrate, respectively,  $\nu$  is the Poisson's ratio and  $\lambda$  and  $A$  are the wavelength and amplitude of the wrinkle, respectively [Figure 6A].

The buckling instability of wrinkles is a fascinating nonlinear mechanical model and is very effective in understanding their formation mechanism from an energy perspective. For a film bonded to a compliant substrate, Huang *et al.* obtained the wavelength and amplitude of the wrinkles for substrates with different moduli and thicknesses by minimizing the energy<sup>[137]</sup>. As shown in Figure 6B, when the strain of the film  $\varepsilon_{\text{film}}$  is less than  $\varepsilon_c$ , the system minimizes at the state  $A = 0$ , and when the strain of the film  $\varepsilon_{\text{film}}$  exceeds  $\varepsilon_c$ , the system wrinkles to an equilibrium amplitude  $A_{\text{eq}}$ . The occurrence of buckling modes may lead to structural and functional failure of the membranes, potentially limiting the performance of materials and is often considered to be avoided. In contrast, stress-driven buckling instability can self-assemble ordered surface

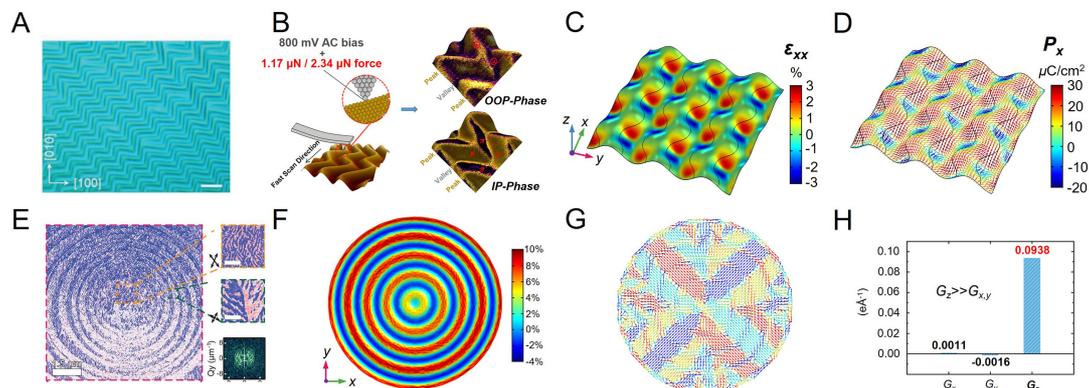


**Figure 6.** (A) A thin film on a compliant substrate undergoes surface wrinkling. (B) Schematic of the total energy of the thin film system as a function of the wrinkle amplitude  $A$  at small (left) and large (right) film strains (reprinted with permission<sup>[137]</sup>. Copyright 2005, Elsevier).

topographies, including sinusoidal, zigzag, labyrinthine, triangular and checkerboard patterns. The physical properties of wrinkles show broad application prospects in the design of flexible electronic devices, the assembly of 3D complex microstructures<sup>[140]</sup>, the morphological control of innovative optoelectronics and integrated systems<sup>[141-143]</sup>, the measurement of mechanical properties of materials<sup>[144,145]</sup> and even medical assistance in diagnosis and treatment<sup>[146]</sup>.

The formation of various wrinkled structures has been reported in thin film systems such as metals<sup>[126]</sup>, graphene<sup>[132]</sup>, organics<sup>[130,131,133,134]</sup>, gels<sup>[147]</sup>, biological tissues<sup>[148]</sup> and more recently in freestanding ferroelectric thin film systems. As shown in Figure 7A, Dong *et al.* successfully fabricated periodic wrinkle-patterned BTO/PDMS membranes based on an as-prepared super-elastic single-crystal freestanding BTO film<sup>[63,64]</sup>. Moreover, finely controlled wrinkle patterns, such as sinusoidal, zigzag and labyrinthine patterns, were obtained by changing the anisotropy and magnitude of the applied stress or adjusting the interfacial adhesion conditions. It is noteworthy that the thickness of the super-elastic BTO film significantly affected the period of the wrinkle pattern. The thicker the BTO film, the larger the wavelength, which also conforms to Equation (10), i.e., the wavelength and period of the wrinkle pattern are proportional to the thickness of the film.

Due to the peculiar morphology of wrinkled ferroelectric films, the strain state is different from the interfacial mismatch strain of conventional epitaxial films. Therefore, a unique ferroelectric domain structure distribution can be generated by applying external loads. For example, the strain field is introduced by a scanning probe, which is quite different from applying out-of-plane strain directly to the epitaxial film, as shown in Figure 7C. Zhou *et al.* found a periodic “braided” in-plane domain superstructure and opposite out-of-plane domains between peaks and valleys through the modulation of scanning probe microscopy (SPM) tip-induced loading forces, as seen in Figure 7B<sup>[64]</sup>. This unique domain depends on the strain state induced by the zigzag wrinkle morphology and the loading of the SPM tip. Due to the periodic “braided-like” strain state, the polarization is deflected to the direction parallel (perpendicular) to the tensile strain (compressive strain)  $\epsilon_{xx}$ , resulting in the formation of the ferroelectric nanodomain structure, as shown in Figure 7D. In addition, some novel wrinkle structures also exist in flexible ferroelectric polymer systems. As shown in Figure 7E, Guo *et al.* found a periodic toroidal “target-like” wrinkle morphology in a flexible ferroelectric polymer poly(vinylidene fluoride-ran-trifluoroethylene) [P(VDF-TrFE)], as well as a peculiar toroidal topological texture using in-plane piezoresponse force microscopy (IP-PFM) measurements<sup>[65]</sup>. The distribution of the toroidal domain structure [Figure 7G] is caused by the strain state induced by the “target-like” wrinkle morphology under external tensile strain, which is a periodically alternating tensile and compressive strain [Figure 7F]. According to this calculation, the electric toroidal moment<sup>[149]</sup>  $G_z$  is much larger than  $G_x$  and  $G_y$ , indicating the existence of in-plane toroidal order



**Figure 7.** (A) Optical microscopy images of wrinkled BTO. The scale bar is 20  $\mu\text{m}$ . (B) Piezoresponse force microscopy (PFM) phase color images of zigzag-wrinkled BTO under scanning force induced by the SPM tip. (C) Distribution of corresponding strain component  $\epsilon_{xx}$  of zigzag-wrinkled BTO by the SPM tip from phase-field simulations considering the flexoelectric effect. (D) Distribution of “braided-like” polarization of zigzag-wrinkled BTO by the SPM tip. The color bar represents the polarization component  $P_x$ . (E) IP-PFM phase image showing the toroidal polar topology of wrinkled P(VDF-TrFE) film. (F and G) The in-plane strain and domain structure of the wrinkled P(VDF-TrFE) under an applied tensile strain of 7.3% from phase-field simulations, respectively. (H) The electric toroidal moments corresponding to the domain structure in (G) illustrate the presence of in-plane topological domains. Panel A reprinted with permission<sup>[63]</sup>. Copyright 2020, Wiley-VCH. Panels B-D reprinted with permission<sup>[64]</sup>. Copyright 2022, American Chemical Society. Panels E-H reprinted with permission<sup>[65]</sup>. Copyright 2021, The American Association for the Advancement of Science.

[Figure 7H]. Therefore, the morphology of freestanding ferroelectric wrinkled films can be developed as a degree of freedom for strain tuning the domains and physical properties of flexible ferroelectric systems.

### 3D nanospring structure of freestanding ferroelectric thin films

Ferroelectric materials display a range of individual polar topological states, including flux-closure domains<sup>[150,151]</sup>, vortices<sup>[152-155]</sup>, skyrmion bubbles<sup>[156,112,157]</sup>, merons<sup>[158]</sup>, center domains<sup>[159]</sup> and sixfold vortex networks<sup>[160]</sup>, as a result of geometrical constraints between structural shape and material interface at the micro/nanoscale. The competition and coupling of elastic, electrostatic and gradient energies can lead to the induction of novel polar topologies that are not stable in conventional bulk ferroelectrics under the combined influence of a sharply increased depolarization field caused by size, noticeable interface and boundary constraint effects. With the demand for the miniaturization and multi-functionalization of functional ferroelectric devices, an increasing number of nanostructures with novel topological ferroelectric domains can be realized through top-down and bottom-up nanofabrication techniques. For example, Shimada *et al.* designed and studied 2D PTO nanostructures (including honeycomb, kagome and star shapes) by establishing a phase-field model based on a 2D Archimedes lattice<sup>[161]</sup>. Furthermore, the polarization was gradually rotated at the junctions of different repeating units in these nano-metamaterials to form a continuous flow pattern.

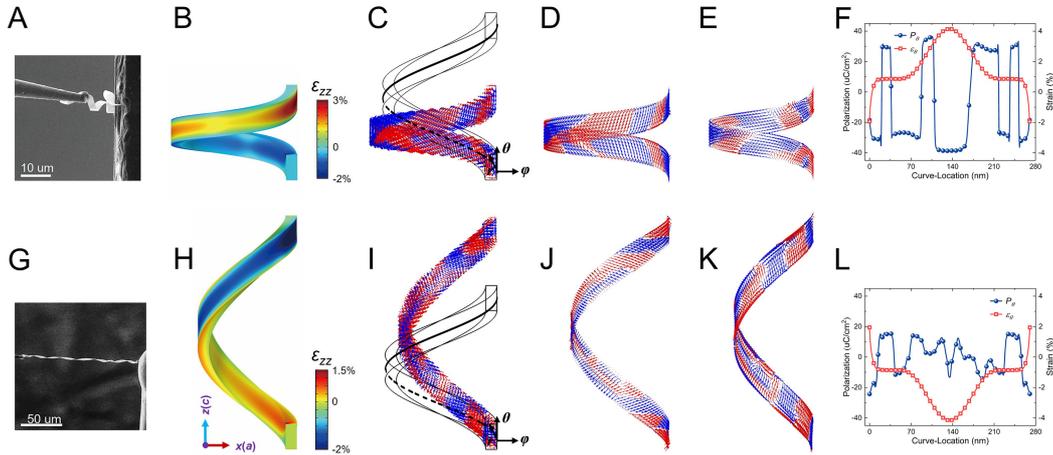
Among the unique nanostructures designed and produced, the emergence of nanosprings has received considerable attention. Nanosprings can achieve enormous amounts of mechanical deformation while maintaining mechanical integrity and are also an essential set of geometries among chiral structures. This 3D helical structure can have broad potential applications in electromechanical devices such as nanoactuators, nanosensors and nanomotors. In contrast to the wrinkles reviewed in the previous section, mechanical buckling-induced self-assembled nanosprings can be obtained by removing the mechanical constraints in the out-of-plane direction and introducing a bilayer structure. Changes in these mechanical conditions enable the system not to be confined to 2D in-plane extended wrinkle deformation but to 3D deformation modes, such as rolling and twisting, leading to the formation of 3D rolled-up structures. This

unique buckling behavior has been utilized in various studies to obtain 3D structures from 2D bilayers, coupled with the characteristic that nanomembranes typically exhibit anisotropic mechanical properties and deform alongside a particular direction. From an energy perspective, the helical shape usually results from the competition between bending and in-plane stretching energy driven by some internal or external force (including surface stress, residual stress, mismatch strain, and so on). The strain gradient in the flexible layer leads to bending along the direction with the smallest Young's modulus<sup>[162,163]</sup> and the twisting of the bilayer structure can be achieved by the strain gradient field introduced by the mismatch strain between the anisotropic bilayers.

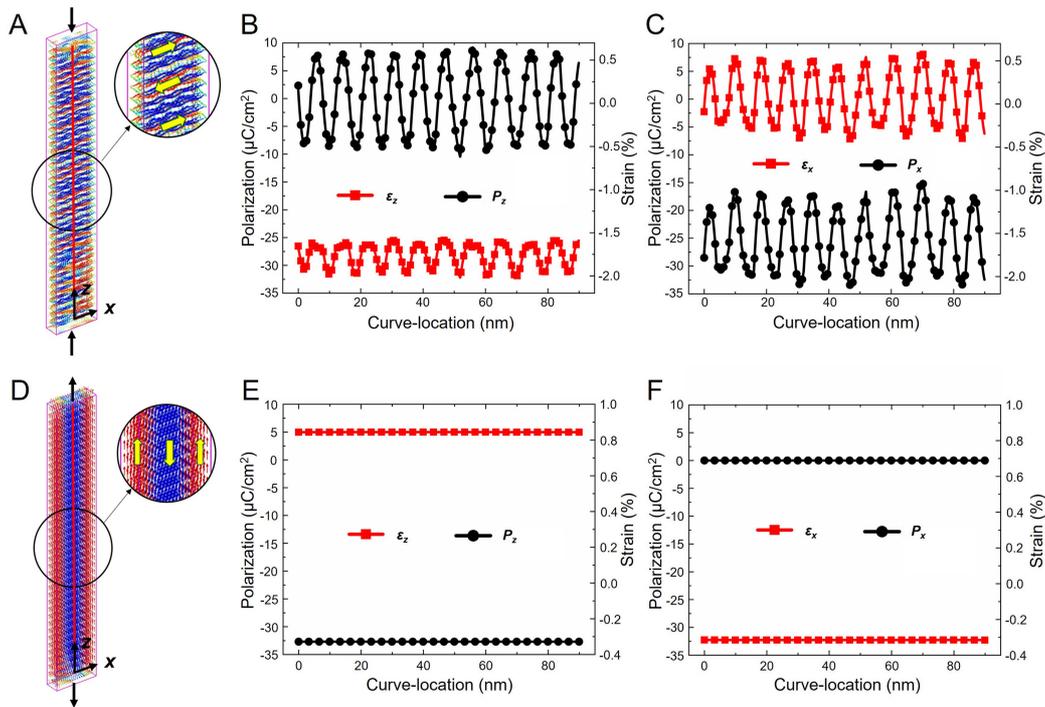
Many helical structures have been found in many inorganic thin film systems<sup>[164]</sup> and have recently been reported in ferroelectric oxides. Despite the fragile ionic or covalent bonds in oxides, Dong *et al.* fabricated self-assembled  $\text{La}_{0.7}\text{Sr}_{0.3}\text{MnO}_3/\text{BaTiO}_3$  (LSMO/BTO) ferroelectric nanosprings with excellent elasticity and recovering capability via a water-peeling off process<sup>[66]</sup>. The BTO nanospring could be stretched or compressed to the geometric limit without breaking failure, thereby achieving a considerable scalability of 500% [Figure 8A and G]. The corresponding bilayer fabrication process with a strain gradient can produce high-quality spring structures of ferroelectric oxides, which have wide applicability. The phase-field simulations reveal that the excellent scalability originates from the continuously rotating ferroelastic domain structures, which provide displacement tolerance and energy to accommodate complex strains of mixed bending and twisting during mechanical deformation. Figure 8B and H show the strain component distribution  $\varepsilon_{zz}$  of nanosprings under compression and elongation, respectively. This unique strain state results in the transition of  $180^\circ$  strip domains distributed around the surface of the ferroelectric nanospring, as shown in Figure 8C and I. For example, during the compression/elongation process, the outer and inner surfaces of the nanospring are subjected to opposite strains, which results in different ferroelectric domain structures on the two surfaces [Figure 8D, E, J and K]. It is noteworthy that the bending moment is the largest in the region farthest laterally from the centerline of the 3D helix (i.e., the middle region of a single helical structure); therefore, the strain effect in this region is more evident. For example, when the nanospring is stretched, the compressive strain on the outer surface of the middle region is more evident than the tensile strain on the inner surface, so the electric dipoles in this region deflected perpendicular to the  $z$ -axis, forming a  $180^\circ$  domain structure in the out-of-plane of the BTO layer.

Figure 8F and L show the relationship between the polarization and the strain distribution on the outer surface of the BTO nanospring under compression and elongation, respectively. When the BTO thin films are twisted into the self-assembled nanosprings, the electromechanical coupling behavior differs from the direct relationship between polarization and strain in the previous ferroelectric film state [Figure 9]. Furthermore, the effect of shear strain is different in the two states. In the previous ferroelectric thin film state, the shear strain has almost no effect on the domain structure; however, when the BTO film is twisted into a nanospring state, the effect of shear strain cannot be ignored. Therefore, the nanospring design provides a novel conceptual framework and platform for the strain engineering of freestanding ferroelectric thin films. Regarding the 3D helical structure, many experimental and theoretical works<sup>[163,165-167]</sup> have reported the shape transition and regulation by external fields of the helical structure. Therefore, the helical structure of ferroelectric oxides can be further regulated in morphology and properties by changing the geometric parameters, modulus ratio and pre-strain of the bilayer film. For example, the mechanical deformation of the nanospring can also be regulated by applying an electron-beam-induced field, which is expected to be applied in flexible nanorobots.

Through the nonlinear mechanical model of Euler buckling, a series of novel functional mechanical structures can be realized, including other self-assembled superstructures (such as origami, kirigami and



**Figure 8.** (A and G) In situ SEM images of the BTO nano-spring in compressive and tensile deformation, respectively. (B-F and H-L) Distribution of the strain component  $\epsilon_{zz}$ , the domain structure, the outer surface domain, the inner surface domain, and the polarization component  $P_0$  and strain distribution  $\epsilon_0$  along the middle line of the outer surface of the BTO nano-spring during compression and stretching, respectively. All panels reprinted with permission<sup>[66]</sup>. Copyright 2022, Wiley-VCH.



**Figure 9.** (A and D) The polarization distribution of BTO freestanding thin films under compressive and tensile deformation, respectively. [(B and C) and (E and F)] The polarization-strain distribution on the centerline of BTO freestanding thin films during compression and elongation, respectively. All panels reprinted with permission<sup>[66]</sup>. Copyright 2022, Wiley-VCH.

textile shapes), in addition to the previously reviewed wrinkled and helical structures. This mechanical modeling strategy based on these self-assembled 3D structure concepts can provide additional and unique ideas and solutions for developing and designing high-performance flexible ferroelectric devices. Furthermore, utilizing external stimuli (such as an external force or electric field) can qualitatively or even quantitatively manipulate the deformation of these mechanically buckling structures, providing a new

approach for strain engineering and domain engineering of freestanding ferroelectric systems.

## CONCLUSION AND OUTLOOK

As reviewed in this article, super-elastic ferroelectric materials are expected to be applied in a wide range of flexible electronic devices, including flexible memories, nanosensors, and nanogenerators. It is essential that ferroelectric materials maintain stable electrical performance under various mechanical deformations, such as stretching, compression, bending and twisting, which involves the dynamic behavior of mesoscopic domain structures in the ferroelectric materials. However, the direct observation of domain structure evolution during continuous deformation of freestanding ferroelectric thin films is challenging for current experimental methods. Moreover, phase-field simulations have become increasingly critical in revealing the super-elasticity of freestanding ferroelectric films and the dynamical behavior of domain structures in different nanostructures. Therefore, the combination of experimental observations and phase-field simulations plays a crucial role in expanding the research and application of super-elastic ferroelectric materials in the field of flexible electronics. To further play the guiding role of theoretical modeling in super-elastic freestanding ferroelectric thin films, the following crucial issues deserve attention and solutions:

***Flexoelectric effect.*** The flexoelectric effect describes the coupling between the electric polarization and strain gradient. Since the strain gradient is inversely proportional to the spatial scale (i.e., the gradient of the strain concerning the spatial coordinate), the flexoelectric effect is size-dependent<sup>[168]</sup>. Therefore, the flexoelectric effect becomes increasingly evident and prominent as the size diminishes, and its contribution to the domain engineering of super-elastic freestanding ferroelectric thin films cannot be ignored. However, the theories and algorithms considering the flexoelectric effect in the phase-field model of super-elastic ferroelectrics still need further verification and improvement. For the freestanding ferroelectric system under mechanical deformation, it is necessary to establish a phase-field model considering the flexoelectric effect to study the origin, enhancement and application of the flexoelectric effect on super-elasticity.

***Design, fabrication and regulation of novel and functional mechanical structures.*** In the regulation and application of freestanding ferroelectric systems, the design and preparation of novel and functional mechanical structures are also the focus of research. The influence of 3D superstructures (e.g., isometric helicoids, kagome shapes and hexagonal honeycombs) on the polarization distribution of ferroelectrics also requires systematic research and analysis.

***Responsive behavior in multiple fields.*** Freestanding ferroelectric thin film systems exhibit several novel topological phenomena and it is essential to demonstrate the response and regulation of these topological structures in multi-physical fields (e.g., individual or mixed applications of mechanical, electric and magnetic fields). In contrast, the response behavior of super-elastic freestanding ferroelectric nanostructures under the external field still needs further research and analysis. For example, the stretching and compressing behavior of ferroelectric nano-springs may be modulated by an electron-beam-induced field, which could have potential applications in the design of flexible nanorobots.

## DECLARATIONS

### Authors' contributions

Conceived and designed the manuscript: Huang HB, Guo CQ

Drafted and revised the manuscript: Huang HB, Guo CQ

### Availability of data and materials

Not applicable.

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### Conflicts of interest

All authors declared that there are no conflicts of interest.

### Ethical approval and consent to participate

Not applicable.

### Consent for publication

Not applicable.

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