

Shear bond strength of universal adhesive systems to a bioactive dentin substitute (Biodentine®) at different time intervals

Sedef Aksoy, Murat Ünal

Department of Pediatric Dentistry, Faculty of Dentistry, Cumhuriyet University, 58140 Sivas, Turkey.

Correspondence to: Dr. Murat Ünal, Department of Pediatric Dentistry, Faculty of Dentistry, Cumhuriyet University, 58140 Sivas, Turkey.
E-mail: gmuratunal@hotmail.com

How to cite this article: Aksoy S, Ünal M. Shear bond strength of universal adhesive systems to a bioactive dentin substitute (Biodentine®) at different time intervals. *Stomatological Dis Sci* 2017;1:116-22.

ABSTRACT

Article history:

Received: 17 May 2017
First Decision: 1 Jun 2017
Revised: 13 Jul 2017
Accepted: 14 Jul 2017
Published: 25 Dec 2017

Key words:

Biodentine®,
compomer,
universal adhesive systems,
shear bond strength

Aim: The aim of this study was to compare the shear bond strength (SBS) of various adhesive systems to a bioactive dentin substitute Biodentine® with different time intervals. **Methods:** Three hundred and fifty cylindrical acrylic blocks with a hole (4 mm diameter and 2 mm height) were prepared. The holes were filled with Biodentine®, and the specimens were allocated into 5 main groups according to waiting times (group 1, 12 min; group 2, 24 h; group 3, 48 h; group 4, 72 h; and group 5, 96 h). All specimens were stored at 37 °C with 100% humidity during the waiting time. Then each group was divided into 7 subgroups of 10 units each: subgroup 1, Prime&Bond NT™; subgroup 2, Single Bond Universal (self-etch mode); subgroup 3, Single Bond Universal (etch and rinse mode); subgroup 4, All-Bond Universal™ (self-etch mode); subgroup 5, All-Bond Universal™ (etch and rinse mode); subgroup 6, G-aenial Universal Bond™ (self-etch mode); and subgroup 7, G-aenial Universal Bond™ (etch-and-rinse mode). After the application of adhesive systems, compomer Dyract XP Bond® was applied over Biodentine® SBSs were measured using a universal testing machine. After the SBS test, the fractured surfaces were examined under a stereomicroscope at 25× magnification, and the data were analyzed with Kruskal-Wallis and Mann-Whitney *U* (with Bonferroni correction) tests. **Results:** Biodentine® exhibits lower shear bond strength values in the 12 min groups. No significant differences were observed between self-etch or etch-and-rinse bonding modes. **Conclusion:** A 24-h waiting period after the mixing of Biodentine® could be useful to obtain higher SBS measurements. Also, similar SBS values were observed for the universal adhesives regardless of application mode.

INTRODUCTION

Mineral trioxide aggregate (MTA) has become a material which attracted attention in vital pulp treatments with its proper biologic characteristics and favorable histological/clinical outcomes^[1,2]. However, MTA has some critical disadvantages like the long

setting time, high resolution during the setting process, staining potential in dental tissues and is difficult to use despite its favorable properties^[3]. New calcium silicate-based cements, including Biodentine®, were developed to overcome these disadvantages.

Biodentine® contains tri- and dicalcium silicates as



This is an open access article licensed under the terms of Creative Commons Attribution 4.0 International License (<https://creativecommons.org/licenses/by/4.0/>), which permits unrestricted use, distribution, and reproduction in any medium, as long as the original author is credited and the new creations are licensed under the identical terms.

For reprints contact: service@oaepublish.com

Quick Response Code:



the main material, calcium carbonate as a filler that improves its mechanical properties and zirconium dioxide as a radiopacifier^[4]. Its liquid component is composed of distilled water, calcium chloride, and a water-soluble polymer. Calcium chloride acts as an accelerator enabling faster setting of the material^[5]. The water-soluble polymer serves to reduce water/cement ratio that increases the material strength^[6]. The most important advantages of Biodentine® over MTA include ease of use, high viscosity, short setting time (12 min) and more favorable physical properties^[7]. Biodentine® also has more developed antibacterial property and a lower cytotoxic effect^[8]. In addition, its microhardness, flexural strength, and compressive strength are higher than those of the other calcium silicate cements and similar to that of dentin^[9].

Besides the biocompatibility, bioactivity, and remineralization abilities of pulp capping materials, the bond strength between restorative and pulp capping materials has great importance for the quality of the filling and the success of the restoration. Regular bonding of compomers to pulp capping materials leads to an adhesive bond that can spread stress equally along the whole adhesion site^[10]. The current adhesive technologies tend to simplify bonding procedures, shorten clinical application time, reduce technical sensitivity by reducing application steps and thereby provide standardization^[11].

Self-etch (SE) adhesive systems were produced in order to eliminate acid etching procedure which is quite a sensitive technique^[12]. These adhesives are easier to use compared to multi-step etch-and-rinse (ER) adhesives. Also, they have a faster application procedure and require less technical sensitivity^[12,13]. The SE technique enables ease of application and reduces contamination with saliva through reducing procedure steps, particularly in children who are difficult to cooperate^[14,15].

A new type of SE adhesive described as “universal”, and “multi-mode” that may be applied both in SE and ER modes has been introduced to the market^[16]. Manufacturers reported that the bonding activity was not compromised when both adhesive techniques are used and also these adhesive systems could also be used for selective etching of enamel margins^[17]. These adhesive systems may be used in both types so as to enable dentists to apply the most proper adhesive protocol to the prepared cavity^[16].

The purpose of this study is to evaluate shear bond strength using four different adhesive systems to Biodentine® which were stored at five different time intervals.

METHODS

Four commercial adhesive systems, Prime&Bond NT™ (PB) (Caulk/Dentsply International Inc., USA), Single Bond Universal (SB) (3M™ ESPE™, USA), All-Bond Universal™ (AB) (Bisco, USA), G-aenial Bond Universal™ (GB) (GC Corporation, Japan) were tested in this study and applied as recommended by the manufacturers. The materials used are listed in Table 1.

Specimen fabrication

A total of 350 acrylic blocks containing a central hole with a 4-mm diameter and a 2-mm height were prepared. Biodentine® (Septodont, Saint-Maur-des-Fosses Cedex, France) was mixed according to the manufacturer's instructions and acrylic blocks were filled with Biodentine® [Figure 1]. Then, the specimens were divided into 5 main groups according to waiting periods: group 1, 12 min; group 2, 24 h; group 3, 48 h; group 4, 72 h; and group 5, 96 h. All specimens stored at 37 °C with 100% humidity during the waiting time.

Then each main group was divided into 7 subgroups of 10 each: subgroup 1, PB; subgroup 2, SB self-etch mode (SB-SE); subgroup 3, SB etch-and-rinse mode (SB-ER); subgroup 4, AB self-etch mode (AB-SE); subgroup 5, AB etch-and-rinse mode (AB-ER); subgroup 6, GB self-etch mode (GB-SE); subgroup 7, GB etch-and-rinse (GB-ER) mode. In each group, the corresponding adhesive system was applied over Biodentine® according to the group's manufacturer's instructions. Following this, a compomer material (Dyract® XP Dentsply DeTrey, Konstanz, Germany) was applied into a cylindrical plastic matrix with an internal diameter of 2 mm and a height of 2 mm. Light curing was administered with a light-emitting diode light curing unit (Elipar™ S 10, 3M ESPE™, St. Paul, MN, USA) with an intensity of 1,200 mW/cm² for 20 s. This procedure was repeated at 24, 48, 72, and 96 h after mixing an additional 70 samples at each time period, respectively.

Shear bond strength test

The polymerized specimens were stored at 100% relative humidity at 37 °C for 24 h. For shear bond strength testing, the specimens were secured in a holder placed on the platen of the testing machine and then sheared with a knife-edge blade on a universal testing machine (LF Plus, LLOYD Instruments, Amatek Inc., UK) at a crosshead speed of 1.0 mm/min. The shear bond strength in MPa was calculated by dividing the peak load at failure with the specimen surface area.

Fracture analysis

The fractured test specimens were examined under a

Table 1: Chemical composition and application procedure of the tested materials

Materials	Composition	Mode/steps of application	
Biodentine Septodent, Saint-Maur-des-Fosses Cedex, France (B08918)	Powder: Tri-calcium silicate, di-calcium silicate, calcium carbonate and oxide filler, iron oxide, zirconium oxide radiopacifier Liquid: calcium chloride accelerator/hydro-soluble polymer water reducing agent	Five doses liquid and powder supplied for 30 s with a mixed amalgamator	
Dyract XP, Dentsply DeTrey, Konstanz, Germany (1404001003)	UDMA, carboxylic acid modified dimethacrylate, TEGDMA, trimethacrylate resin, camphorquinone, ethyl-4-dimethylaminobenzoate, BHT, UV stabiliser, strontium-alumino-sodium-fluorophosphor-silicate glass, highly dispersed silicon dioxide, strontium fluoride, iron oxide and titanium dioxide pigments (average filler size: 0.8, filler volume 47%)		
Condac 37 (281014)	37% phosphoric acid deionized water	Self-etch strategy	Etch-rinse strategy
Prime & BondNT (PB), Caulk/Dentsply International Inc., USA (1407000539)	Di- and trimethacrylate resins Dipentaerythritol penta acrylate monophosphate UDMA Nanofillers Amorphous silicon dioxide Photoinitiators Stabilisers Cetylamine hydrofluoride Acetone		1. Apply etchant for 15 s 2. Rinse for 10 s 3. Scrub adhesive for 20 s 4. Air-thin for 5 s 5. Light-cure for 10 s
Single Bond Universal (SB), 3 M Espe, St. Paul, MN, USA (533701)	10-MDP phosphate monomer, Vitrebond copolymer, HEMA, BISGMA, dimethacrylate resins filler, silane, initiators, ethanol, water	1. Apply the to the Biodentine and rub it in for 20 s 2. Gently air-dry the adhesive for approximately 5 s for the solvent to evaporate 3. Light cure for 10 s	1. Apply etchant for 15 s 2. Rinse for 10 s 3. Air dry 5 s 4. Apply adhesive as for the self-etch mode
All-Bond Universal (AB), Bisco Schaumburg, IL, USA (1300009232)	10-MDP phosphate monomer, HEMA, BISGMA, ethanol	1. Apply 2 separate coats of adhesive, scrubbing the preparation with a microbrush for 10-15 s per coat. Do not light cure between coats 2. Evaporate excess solvent by thoroughly air-drying with an air syringe for at least 10 s, there should be no visible movement of the material. The surface should have a uniform glossy appearance 3. Light cure for 10 s	1. Apply etchant for 15 s 2. Rinse thoroughly 3. Remove excess water with absorbent pellet or high volume suction for 1-2 s 4. Apply adhesive as for the self-etch mode
G-aenial Bond (GB), GC, Tokyo, Japan (1403111)	Acetone, dimethacrylate, TEGDMA, 4-MET, phosphoric acid ester monomer, silicon dioxide, photo initiator	1. Apply using a microbrush 2. Leave undisturbed for 10 s after the end of application 3. Dry thoroughly for 5 s with oil free air under maximum air pressure 4. Light-cure for 10 s	1. Apply etchant for 15 s 2. Rinse for 5 s and gently dry 3. Apply adhesive as for the self-etch mode

stereomicroscope (Stemi DV4: Carl Zeiss, Gottingen, Germany) at a magnification of 25 \times . Specimen fractures were classified as follows: cohesive failure exclusively within Biodentine®, cohesive failure exclusively within compomer, the adhesive failure that occurred at the Biodentine®-compomer interface; or mixed failure when two modes of failure happened simultaneously [Figure 2]. Fracture analysis was performed by a single observer who was completely uninformed about the experimental groups. For the scanning electron microscope (SEM) analyses, samples randomly selected from the 12 min and 96 h groups of the failure specimens. The failure surfaces were sputter-coated with gold using a Sputter Coater, and specimens were analyzed with a SEM (Zeiss Evo LS10, Oberkochen, Germany). The significance of the difference between

groups with regard to median shear bond strength was analyzed with Mann Whitney *U* test when there were two independent groups and the with Kruskal-Wallis test when there were more than two independent groups. A *P* level of < 0.05 was accepted as statistically significant. However, Bonferroni correction was done in order to control type 1 error in all potential multi-comparisons.

RESULTS

Mean shear bond values and standard deviations are shown in Table 2. The samples stored for 12 min showed statistically significantly lower shear bond values compared to the other time periods, except the PB and AB-SE groups. However, there was no

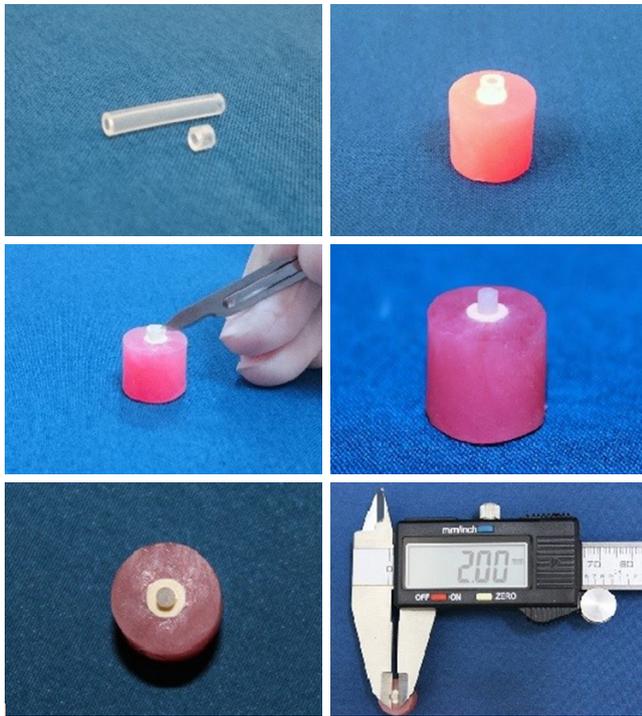


Figure 1: Preparation of working samples and application of compomer

significant difference between specimens stored 24 h, 48 h, 72 h and 96 h.

No statistically significant differences were found between all the adhesive systems at each of the 5 time intervals (12 min, 24 h, 48 h, 72 h and 96 h). In addition, statistically significant differences could not be found between SE and ER modes of universal adhesive systems [Table 2]. Table 3 shows the fracture modes of the experimental groups.

In SEM and stereomicroscope analysis while more superficial cohesive failures were observed in Biodentine® in the 12 min groups, deeper cohesive failures were seen in the 96 h groups. Also, the surface failures of specimens stored for 12 min were seen to be more irregular and porous; the surface structure

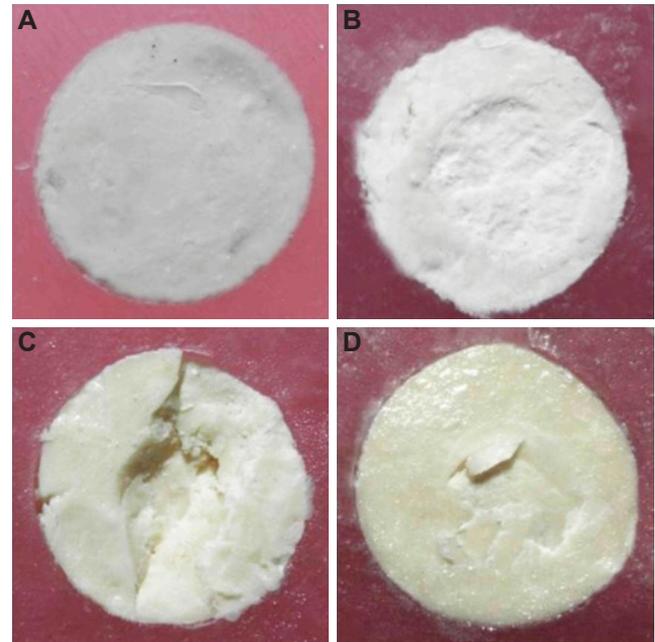


Figure 2: Steriomicroscopic imaging of the failure modes. (A) Adhesive failure; (B) superficial cohesive failure in Biodentine; (C) deeper cohesive failure in Biodentine; (D) mix failure

was seen to be more regular and smooth in the 96 h groups [Figure 3].

DISCUSSION

Biodentine® was put on the market in 2010, and it was recommended to be used as a dentin substitute in addition to its use in indications similar to ProRoot® MTA (e.g. pulp capping, perforation repair, apexification and as root-end filling)^[18]. Biodentine® was reported to have more developed mechanical properties than ProRoot® MTA and Angelus® MTA, besides its biocompatibility and short setting time^[19,20].

The manufacturer states that setting time of Biodentine® is 12 min and final restoration may be completed in the same appointment^[21]. Biodentine® was reported to set in a shorter time than MTA, as its liquid contains calcium chloride and its powder contains calcium

Table 2: Mean shear bond strength values (MPa) and standard deviations of each group ($n = 10$)

	Prime Bond	Single Bond-SE	Single Bond-ER	All Bond-SE	All Bond-ER	G-aenial Bond-SE	G-aenial Bond-ER	P value [†]
12 min	9.39 (4.34)	10.14 (3.58)	10.17 (2.41)	10.08 (2.86)	10.58 (2.71)	10.81 (2.73)	10.28 (2.09)	0.821
24 h	12.09 (2.71)	14.26 (2.11) ^a	13.66 (3.16) ^a	12.58 (1.41)	13.11 (3.07) ^c	15.74 (5.28) ^c	14.97 (3.20) ^c	0.029
48 h	12.30 (2.79)	12.71 (1.74) ^a	12.98 (3.47) ^c	12.36 (2.91)	13.12 (3.28) ^c	14.90 (2.30) ^c	14.19 (3.13) ^c	0.032
72 h	12.34 (1.13)	13.00 (2.81) ^b	13.18 (1.71) ^c	12.04 (2.48)	12.67 (2.88) ^c	14.17 (4.01) ^c	13.63 (2.38) ^c	0.207
96 h	12.50 (1.97)	12.98 (3.07) ^a	12.62 (2.48) ^c	12.62 (2.36)	13.06 (2.23) ^c	13.88 (2.83) ^c	13.01 (3.03) ^c	0.536
P value [‡]	0.016	0.002	< 0.001	0.022	0.006	< 0.001	< 0.001	

[†]When waiting periods kept constant, comparisons between materials Kruskal-Wallis test, according to the Bonferroni correction for $P < 0.010$ results was accepted statistically significant; [‡]comparisons between waiting periods in materials, Kruskal-Wallis test, according to the Bonferroni correction for $P < 0.0071$ results was accepted statistically significant; ^astatistically significant difference vs. 12 min ($P < 0.001$); ^bstatistically significant difference vs. 12 min ($P = 0.005$); ^caccepted statistically significant differences vs. 12 min. SE: self etch mode; ER: etch and rinse mode

value was observed in the 24 h GB-SE group. The highest bond strength values were obtained with the GB group, although the values were statistically insignificant. This result may be associated with GB's containing acetone as a solvent which has a higher vapor pressure. Acetone may be easily removed from the adhesion surface and may provide higher bond strength by facilitating monomer diffusion due to its high vapor pressure^[27]. Lower shear bond strength was detected in groups with PB, another acetone-containing adhesive system, compared to the other groups. We note that high molecular weight monomers like urethane dimethacrylate and dipenta erythritol penta acrylate monophosphate in composition of PB have led to a decrease in bond strength values through reducing the diffusion capacity of the adhesive^[29].

Applying adhesive systems in either SE or ER was seen not to have a statistically significant effect on bond strength in the present study. This result is similar to the results of the study of Hanabusa *et al.*^[16], Marchesi *et al.*^[17], and Chen *et al.*^[30], who also reported that using SE or ER technique does not statistically significantly influence bond strength. Hashem *et al.*^[25] reported that similar bond strength values between SE and ER modes might be due to the porous structure of the Biodentine® surface, which may have eliminated the difference between SE and ER techniques. In addition, Biodentine® which has alkaline properties may reduce the effect of bonding techniques by buffering their acidity^[25].

In the present study, the most of the specimens exhibited cohesive failure in Biodentine®. The least common of the observed types of failure was adhesive. This result reflects the inner cohesion power of the cohesive rather than the real interfacial bond strength of the adhesive resin and the material. Cohesive failures in restorative material or dentin may be due to the low internal resistance of the material or the bond strength being greater than the material's internal resistance^[31].

In SEM and stereomicroscope images, while more superficial cohesive failures are observed within Biodentine® in 12 min groups [Figure 2A], deeper cohesive failures were seen in 96 h groups [Figure 2B]. It may be suggested that the superficial failure in 12 min groups may result from polymerization shrinkage of the compomer placed on Biodentine®. The curing contraction of the compomer may lead to stresses, resulting in premature failures in weak Biodentine® which is in early sensitive phase. This finding should be addressed carefully, as it may affect decisions to immediately place the restoration on Biodentine®^[25].

In conclusion, based on the data of this study, it may

be concluded that before applying compomer material on Biodentine®, a waiting period of at least 24 h can be useful to obtain high SBS values. It may be suggested that sufficient bonding performance may also be obtained without an acid etching procedure, as universal adhesive systems applied on Biodentine® show similar bond values in SE and ER modes. In this way, ease of use is provided for particularly uncooperative pediatric patients by the reduced number of procedure steps, and the risk of contamination with saliva is also reduced.

DECLARATIONS

Acknowledgments

We thank Dr. Jon Wagner for his contribution in language editing.

Authors' contributions

Manuscript's preparation: S. Aksoy

Manuscript's review: M. Ünal

Financial support and sponsorship

This study is supported by CÜBAP (DİŞ-142).

Conflicts of interest

The authors deny any conflicts of interest related to this study.

Patient consent

Not applicable.

Ethics approval

This study has started to work after the approval of ethics committee, Faculty of Medicine, Cumhuriyet University Faculty of Medicine Clinical Research and Ethics Committee (2014-03/16).

REFERENCES

1. Asgary S, Eghbal MJ. Treatment outcomes of pulpotomy in permanent molars with irreversible pulpitis using biomaterials: a multi-center randomized controlled trial. *Acta Odontol Scand* 2013;71:130-6.
2. Eghbal MJ, Asgary S, Baglue RA, Parirokh M, Ghoddusi J. MTA pulpotomy of human permanent molars with irreversible pulpitis. *Aust Endod J* 2009;35:4-8.
3. Antunes Bortoluzzi E, Juárez Broon N, Antonio Hungaro Duarte M, de Oliveira Demarchi AC, Monteiro Bramante C. The use of a setting accelerator and its effect on pH and calcium ion release of mineral trioxide aggregate and white Portland cement. *J Endod* 2006;32:1194-7.
4. Camilleri J. Investigation of Biodentine as dentine replacement material. *J Dent* 2013;41:600-10.
5. Bortoluzzi EA, Broon NJ, Bramante CM, Felipe WT, Tanomaru Filho M, Esberard RM. The influence of calcium chloride on the setting time, solubility, disintegration, and pH of mineral trioxide aggregate and white Portland cement with a radiopacifier. *J Endod* 2009;35:550-4.
6. Grech L, Mallia B, Camilleri J. Investigation of the physical properties of tricalcium silicate cement-based root-end filling materials. *Dent*

- Mater* 2013;29:e20-8.
7. Nowicka A, Lipski M, Parafiniuk M, Sporniak-Tutak K, Lichota D, Kosierkiewicz A, Kaczmarek W, Buczkowska-Radlińska J. Response of human dental pulp capped with biodentine and mineral trioxide aggregate. *J Endod* 2013;39:743-7.
 8. Shayegan A, Jurysta C, Atash R, Petein M, Abbeele AV. Biodentine used as a pulp-capping agent in primary pig teeth. *Pediatr Dent* 2012;34:e202-8.
 9. Laurent P, Aubut V, About I. Development of a bioactive Ca₃SiO₅ based posterior restorative material (Biodentine™). Biocompatibility or cytotoxic effects of dental composites. Oxford: Coxmoor; 2009. p. 195-200.
 10. Oskoe SS, Kimyai S, Bahari M, Motahari P, Eghbal MJ, Asgary S. Comparison of shear bond strength of calcium-enriched mixture cement and mineral trioxide aggregate to composite resin. *J Contemp Dent Pract* 2011;12:457-62.
 11. Van Meerbeek B, De Munck J, Yoshida Y, Inoue S, Vargas M, Vijay P, Van Landuyt K, Lambrechts P, Vanherle G. Buonocore memorial lecture. Adhesion to enamel and dentin: current status and future challenges. *Oper Dent* 2003;28:215-35.
 12. Van Meerbeek B, Yoshihara K, Yoshida Y, Mine A, De Munck J, Van Landuyt KL. State of the art of self-etch adhesives. *Dent Mater* 2011;27:17-28.
 13. Perdigão J, Muñoz MA, Sezinando A, Luque-Martinez IV, Staichak R, Reis A, Loguercio AD. Immediate adhesive properties to dentin and enamel of a universal adhesive associated with a hydrophobic resin coat. *Oper Dent* 2014;39:489-99.
 14. Croll TP. Simplified resin-based composite sealant. *ASDC J Dent Child* 2000;67:182-5.
 15. Shimada Y, Senawongse P, Harnirattisai C, Burrow MF, Nakaoki Y, Tagami J. Bond strength of two adhesive systems to primary and permanent enamel. *Oper Dent* 2002;27:403-9.
 16. Hanabusa M, Mine A, Kuboki T, Momoi Y, Van Ende A, Van Meerbeek B, De Munck J. Bonding effectiveness of a new 'multi-mode' adhesive to enamel and dentine. *J Dent* 2012;40:475-84.
 17. Marchesi G, Frassetto A, Mazzoni A, Apolonio F, Diolosà M, Cadenaro M, Di Lenarda R, Pashley DH, Tay F, Breschi L. Adhesive performance of a multi-mode adhesive system: 1-year in vitro study. *J Dent* 2014;42:603-12.
 18. Setbon HM, Devaux J, Iserentant A, Leloup G, Leprince JG. Influence of composition on setting kinetics of new injectable and/or fast setting tricalcium silicate cements. *Dent Mater* 2014;30:1291-303.
 19. Laurent P, Camps J, De Méo M, Déjou J, About I. Induction of specific cell responses to a Ca₃SiO₅-based posterior restorative material. *Dent Mater* 2008;24:1486-94.
 20. Kayahan MB, Nekoofar MH, McCann A, Sunay H, Kaptan RF, Meraji N, Dummer PM. Effect of acid etching procedures on the compressive strength of 4 calcium silicate-based endodontic cements. *J Endod* 2013;39:1646-8.
 21. Rathinam E, Rajasekharan S, Chitturi RT, Declercq H, Martens L, De Coster P. Gene expression profiling and molecular signaling of various cells in response to tricalcium silicate cements: a systematic review. *J Endod* 2016;42:1713-25.
 22. Dawood AE, Manton DJ, Parashos P, Wong R, Palamara J, Stanton DP, Reynolds EC. The physical properties and ion release of CPP-ACP-modified calcium silicate-based cements. *Aust Dent J* 2015;60:434-44.
 23. Jang YE, Lee BN, Koh JT, Park YJ, Joo NE, Chang HS, Hwang IN, Oh WM, Hwang YC. Cytotoxicity and physical properties of tricalcium silicate-based endodontic materials. *Restor Dent Endod* 2014;39:89-94.
 24. Odabaş ME, Bani M, Tirali RE. Shear bond strengths of different adhesive systems to biodentine. *Scient World J* 2013;2013:626103.
 25. Hashem DF, Foxtan R, Manoharan A, Watson TF, Banerjee A. The physical characteristics of resin composite-calcium silicate interface as part of a layered/laminate adhesive restoration. *Dent Mater* 2014;30:343-9.
 26. Kaup M, Dammann CH, Schafer E, Dammaschke T. Shear bond strength of Biodentine, ProRoot MTA, glass ionomer cement and composite resin on human dentine ex vivo. *Head Face Med* 2015;11:14.
 27. Atabek D, Sillelioglu H, Olmez A. Bond strength of adhesive systems to mineral trioxide aggregate with different time intervals. *J Endod* 2012;38:1288-92.
 28. Altunsoy M, Tanriver M, Ok E, Kucukyilmaz E. Shear bond strength of a self-adhering flowable composite and a flowable base composite to mineral trioxide aggregate, calcium-enriched mixture cement, and Biodentine. *J Endod* 2015;41:1691-5.
 29. Duarte Pde B, da Silva EM. Nanoleakage phenomenon on deproteinized human dentin. *J Appl Oral Sci* 2007;15:285-91.
 30. Chen C, Niu LN, Xie H, Zhang ZY, Zhou LQ, Jiao K, Chen JH, Pashley DH, Tay FR. Bonding of universal adhesives to dentine--old wine in new bottles? *J Dent* 2015;43:525-36.
 31. el-Kalla IH, Garcia-Godoy F. Bond strength and interfacial micromorphology of compomers in primary and permanent teeth. *Int J Paediatr Dent* 1998;8:103-14.