

1 **Supplementary Material**

2
3 **A molecular dynamics assisted insight on damping enhancement in carbon fiber**
4 **reinforced polymer composites with oriented multilayer graphene oxide coatings**

5
6 **Muhan Zhang¹, Yalin Yu², Li Li³, Helezi Zhou¹, Luyang Gong¹, Huamin Zhou¹**

7
8 ¹State Key Laboratory of Material Processing and Die & Mold Technology, School of
9 Materials Science and Engineering, Huazhong University of Science and Technology,
10 Wuhan 430074, Hubei, China.

11 ²Aerospace Research Institute of Materials & Processing Technology, Beijing 100076,
12 China.

13 ³State Key Laboratory of Intelligent Manufacturing Equipment and Technology, School
14 of Mechanical Science and Engineering, Huazhong University of Science and
15 Technology, Wuhan 430074, Hubei, China.

16
17 **Correspondence to:** Assoc. Prof. Helezi Zhou, School of Materials Science and
18 Engineering, Huazhong University of Science and Technology, 1037, Luoyu Road,
19 Hongshan District, Wuhan 430074, Hubei, China. E-mail: Helezizhou@hust.edu.cn;
20 Prof. Huamin Zhou, School of Materials Science and Engineering, Huazhong University
21 of Science and Technology, 1037, Luoyu Road, Hongshan District, Wuhan 430074,
22 Hubei, China. E-mail: Hmzhou@hust.edu.cn

23 **Structural optimization**

24 **Figure S1** shows the energy optimization results of DGEBA/TETA unit. After a series of energy
25 minimization, the total potential energy and nonbond energy no longer exhibit significant fluctuations
26 and tend to converge. The premature auto-kill in Newton interaction means that the molecular structure
27 has reached its optimal state. In addition, a 500-ps NVT dynamics was further applied to eliminate
28 residual stress inside the cell, causing relaxation of polymer segments. The stability of energy can also be
29 observed during this stage.

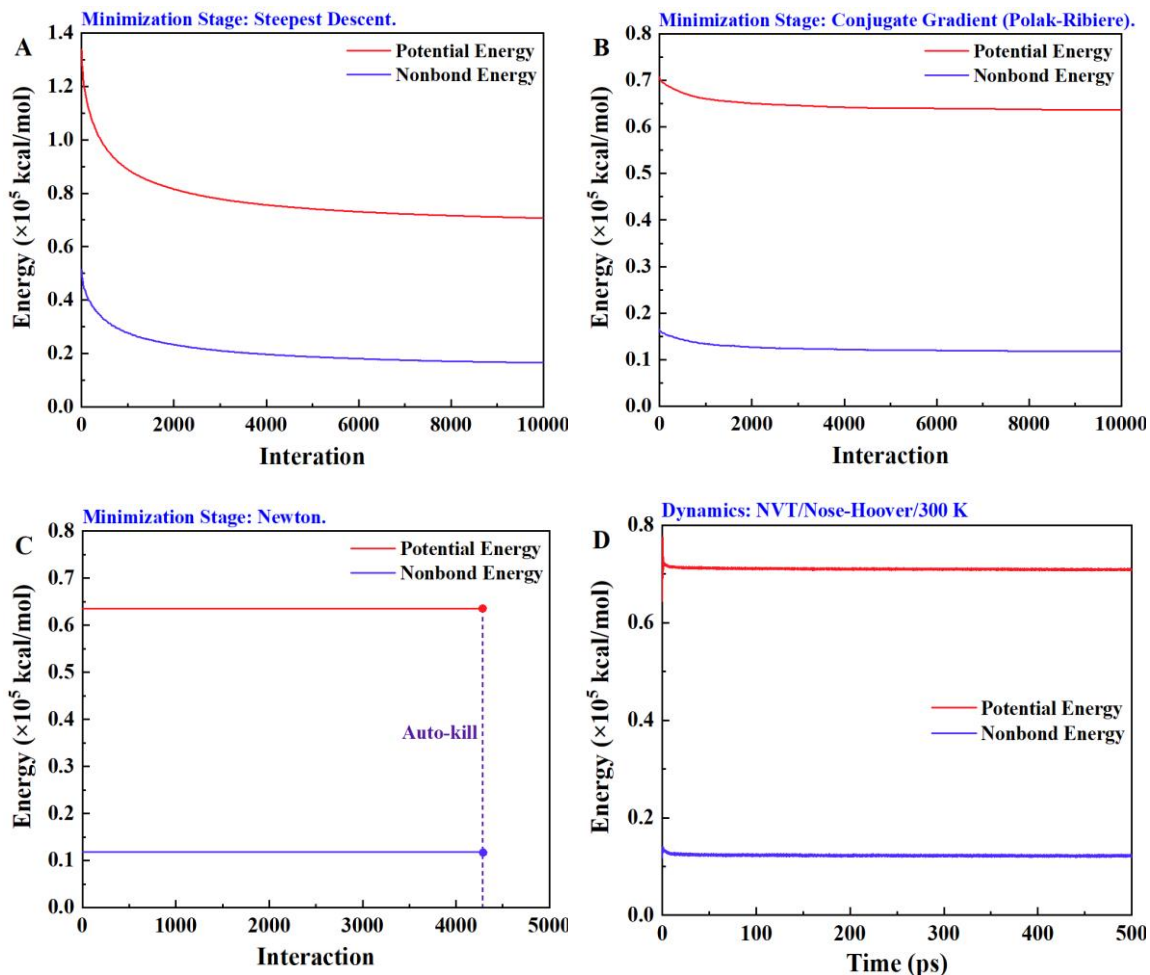


Figure S1. Structural optimization of EDGBA/TETA epoxy unit: (A) Steepest Descent method ($\times 1000$ steps), (B) Conjugate Gradient (Polak-Ribiere) method ($\times 1000$ steps), (C) Newton method ($\times 1000$ steps) and (D) a 500-ps NVT dynamics process under 300 K.

30 Fundamental stretching frequency

31 The fundamental stretching frequency of the atomistic model was investigated using a standard free
 32 vibration method. In detail, the system was initially equilibrated at 300 K using an NVT ensemble ($\Delta t =$
 33 1 fs). The atoms at both ends of the model along the y-axis were fixed. Subsequently, the ensemble
 34 transitioned to a micro-canonical condition (NVE), wherein the total energy of the system remained
 35 constant. Following this, a force was applied to one side of the fixed part to induce a 2% elongation of
 36 the box in the y direction. Upon removing the force, the unrestrained atoms oscillated freely. The
 37 resonant frequency of the system was determined by conducting a fast Fourier transform on the time
 38 response of the center of mass (COM).

39 The temporal response of the displacement of the COM (X_{com}) is monitored in **Figure S2A**, and the
 40 resonant frequency of the system was then obtained from the Fast Fourier transform of the time response
 41 of the X_{com} , as shown in **Figure S2B**. As can be seen, the values of the fundamental stretching frequency
 42 for the D-CFRP_{0LGO}, D-CFRP_{4LGO} and D-CFRP_{8LGO} groups were 2.467 THz, 2.533 THz, and 2.633 THz,
 43 respectively.

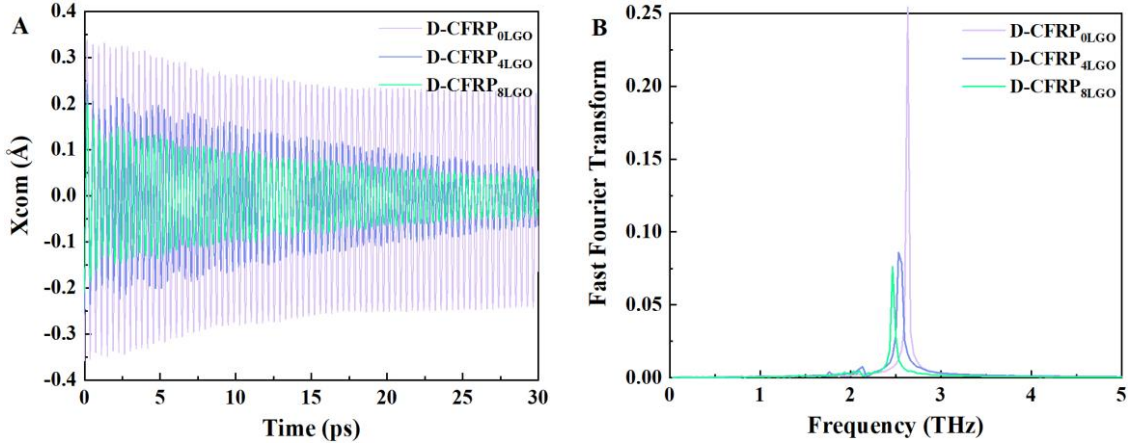


Figure S2. Simulation results obtained by free vibration method: (A) the relationship between the displacement of the centroid along the y-axis and the vibration time, (B) Fast Fourier transform of the X_{com} -time response.

44 Frequency/Temperature dependence of Q factors

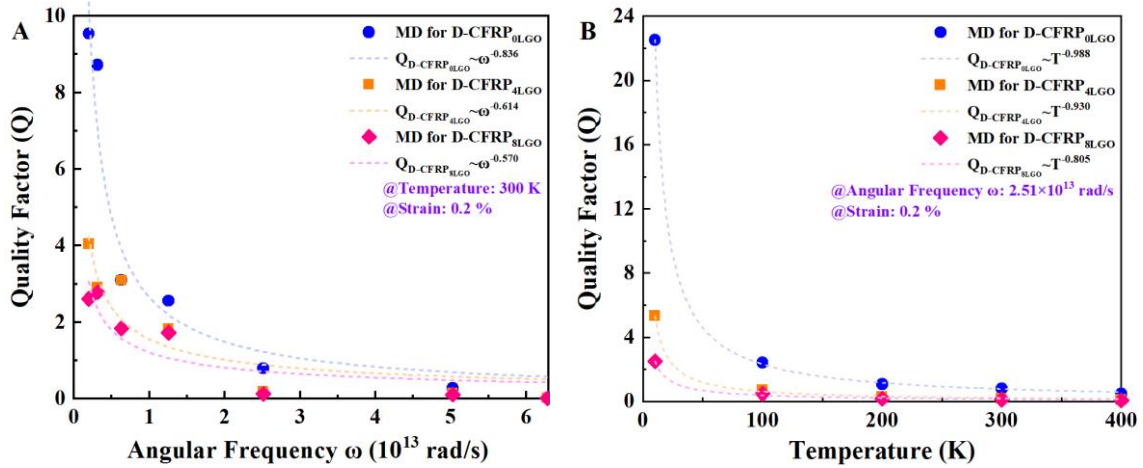


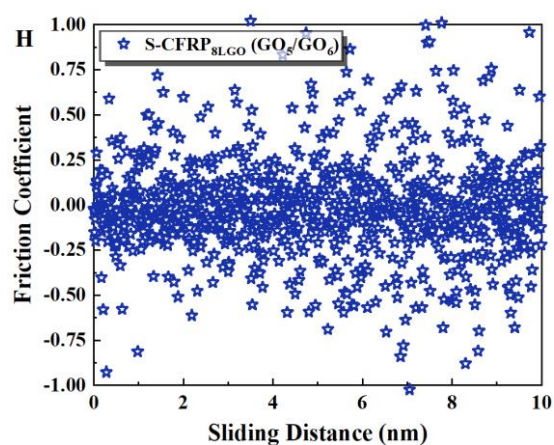
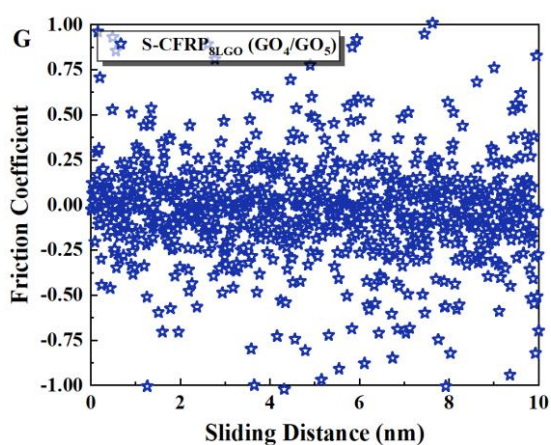
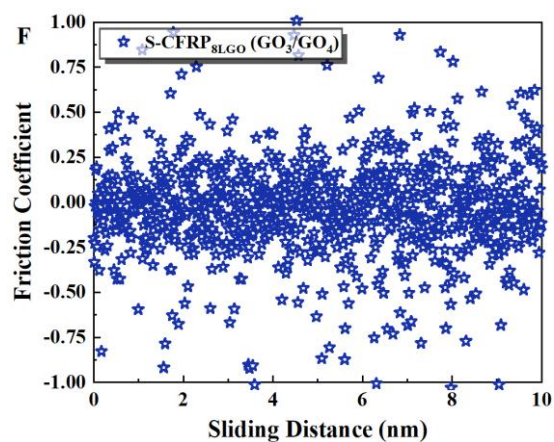
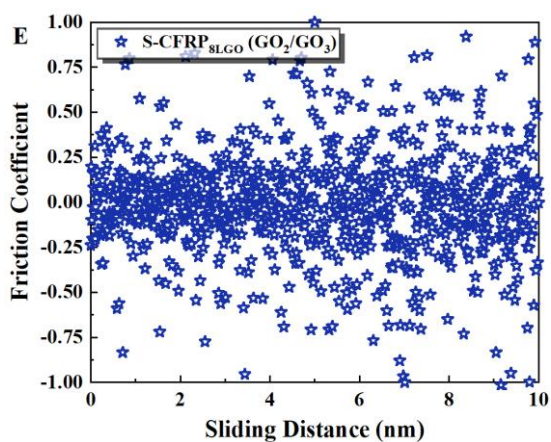
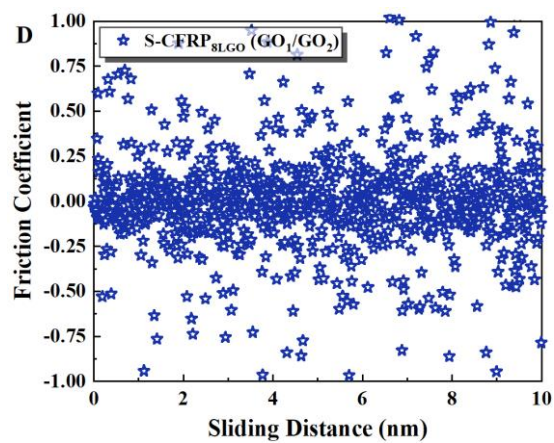
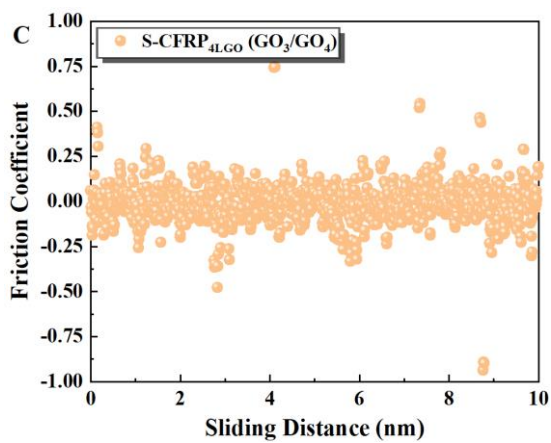
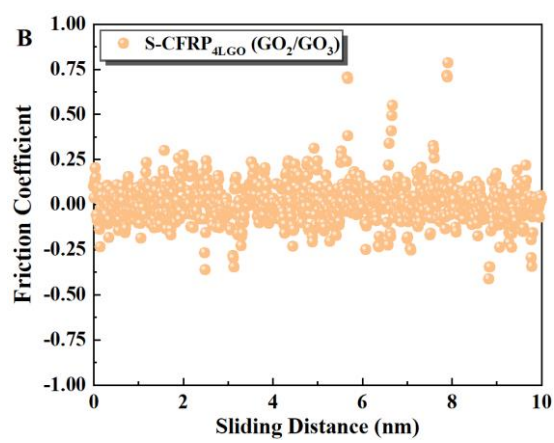
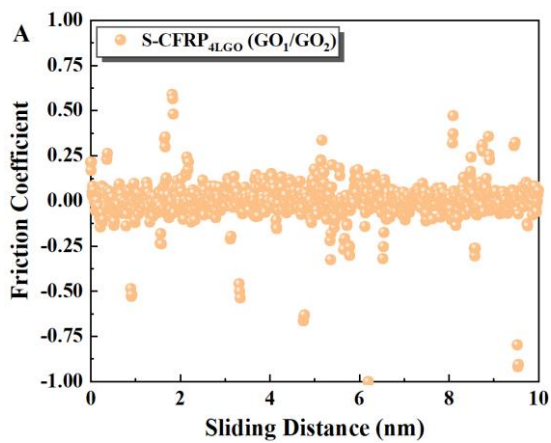
Figure S3. (A) Frequency dependence and (B) Temperature dependence of Q factors for the CFRP systems.

45 Dynamic friction coefficient between GO layers

46 Interlayer slip behavior of GO film by external vibration is highly correlated with the improvement of
 47 damping performance. The interface friction of graphene nanomaterials has been proposed as an
 48 important energy dissipation pathway^[1-2]. Herein, the trajectory of atoms and forces generated in the
 49 sliding direction have been recorded and used for calculating the dynamic friction coefficient (μ), which
 50 is expressed as follow:

$$\mu = \frac{f}{F_n} \quad (S1)$$

51 where the friction force f is obtained by summing the force acting on the adjacent GO layers along the
 52 sliding direction and F_n is the normal force acting on the adjacent GO layers along the z direction.
 53 **Figure S4** shows the calculated μ for each CFRP system. In details, as the thickness of the coating
 54 increases, μ between the sheets gradually diverging during the sliding process. It means that the dynamic
 55 friction force inside the multi-layer GO is higher, which can consume more mechanical energy.



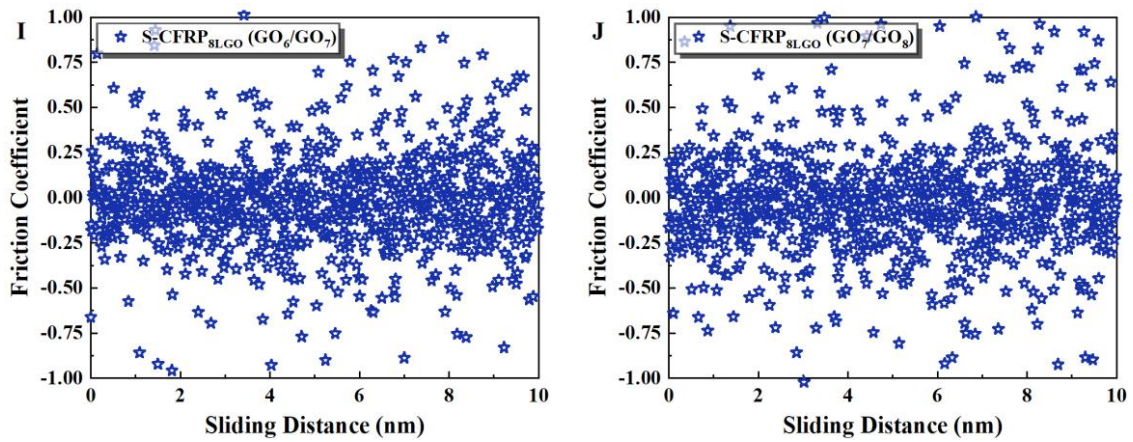


Figure S4. Dynamic friction coefficient of various adjacent GO layers from two CFRP models (A-C) S-CFRP_{4LGO} and (D-J) S-CFRP_{8LGO}. The schematic diagrams of GO₁, GO₂, GO₃, GO₄ in S-CFRP_{4LGO} and GO₁, GO₂, GO₃, GO₄, GO₅, GO₆, GO₇, GO₈ in S-CFRP_{8LGO} have been shown in **Figure 9A**.

56

57 REFERENCES

- 58 1. Suhr J, Koratkar NA. Energy dissipation in carbon nanotube composites: a review. *J Mater Sci.*
 59 2008;43(13):4370-4382. [DOI:10.1007/s10853-007-2440-x]
- 60 2. Zhang XC, Peng HX, Limmack AP, Scarpa F. Viscoelastic damping behaviour of cup stacked
 61 carbon nanotube modified epoxy nanocomposites with tailored interfacial condition and
 62 re-agglomeration. *Compos Sci Technol.* 2014;105:66-72.
 63 [DOI:https://doi.org/10.1016/j.compscitech.2014.09.020]

64