Supplementary Information for

Assessment of the impact of sampler housing on indoor passive air sampler measurements of SVOCs

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Supplementary Table 1. Overview of active and passive sampler deployments

Sampling date	Length of passive sampling (days)	Active low-vol sampler - Leckel PM1		Active low-vol sampler - Leckel PM10		Passive samplers		
		Time (h)	Sample volume (m^3)	Time (h)	Sample volume (m^3)	Double bowl samplers (number of replicates collected)	Single bowl samplers (number of replicates collected)	No bowl samplers (number of replicates collected)
2014-09-12	7	150	329.79	150	330.02	3	3	0
2014-09-19	14	143	316.44	143	316.36	3	3	3
2014-09-26	21	126	276.91	126	276.9	3	3	3
2014-10-03	28	126	277.81	126	277.89	3	3	3
2014-10-10	35	124	272.73	124	272.79	3	3	3
2014-10-17	42	126	274.93	126	274.85	3	3	3
2014-10-24	49	126	276.83	126	276.97	3	3	3
2014-10-31	56	124	278.36	124	278.31	3	3	3
2014-10-31	28	-	-	-	-	3	3	0

Supplementary Table 2. Targeted compounds and abbreviations used. Octanol-air partitioning coefficients are included for compounds with > 50% for which sampling rate calculations were done

Compound class	Abbreviation	Name	CAS Number	InChIKey	$\log K_{OA}$ (OPERA)[1]	Used $\log K_{OA}$[2]
PCB	PCB 9	2,5-Dichlorobiphenyl	34883-39-1	KKQWHYGECTYFIA-UHFFFAOYSA-N	7.41885	7.41885
PCB	PCB 11	3,3'-Dichlorobiphenyl	2050-67-1	KTXUOWUHFLBZPW-UHFFFAOYSA-N	7.41885	7.41885
PCB	PCB 28	2,4,4'-Trichlorobiphenyl	7012-37-5	BZTYNSQSZHARAZ-UHFFFAOYSA-N	7.78147	7.78147
PCB	PCB 52	2,2',5,5'-Tetrachlorobiphenyl	35693-99-3	HCWZEPKLWVAEOV-UHFFFAOYSA-N	8.49	8.49

Compound class	Abbreviation	Name	CAS Number	InChIKey	$logK_{OA}$ (OPERA)[1]	Used $logK_{OA}$[2]
PCB	PCB 101	2,2',4,5,5'-Pentachlorobiphenyl	37680-73-2	LAHWLEDBADHJGA-UHFFFAOYSA-N	8.96003	8.96003
PCB	PCB 118	2,3',4,4',5-Pentachlorobiphenyl	31508-00-6	IUTPYMGCWINGEY-UHFFFAOYSA-N	9.24	
PCB	PCB 138	2,2',3,4,4',5'-Hexachlorobiphenyl	35065-28-2	RPUMZMSNLZHIGZ-UHFFFAOYSA-N	9.80	
PCB	PCB 153	2,2',4,4',5,5'-Hexachlorobiphenyl	35065-27-1	MVWHGTYKUMDIHL-UHFFFAOYSA-N	9.73319	9.73319
PCB	PCB 180	2,2',3,4,4',5,5'-Heptachlorobiphenyl	35065-29-3	WBHQEUPUMONIKF-UHFFFAOYSA-N	9.94	
OCP	PeCB	Pentachlorobenzene	608-93-5	CEOCDNVZRAIOQZ-UHFFFAOYSA-N	6.48809	6.48809
OCP	HCB	Hexachlorobenzene	118-74-1	CKAPSXZOOQJIBF-UHFFFAOYSA-N	7.37397	7.37397
OCP	a-HCH	alpha-hexachlorocyclohexane	319-84-6	JLYXXMFPNIAWKQ-SHFUYGGZSA-N	8.09186	8.09186
OCP	b-HCH	beta-hexachlorocyclohexane	319-85-7	JLYXXMFPNIAWKQ-CDRYSYESSA-N	8.09	
OCP	g-HCH	gamma-hexachlorocyclohexane	58-89-9	JLYXXMFPNIAWKQ-GNIYUCBRSA-N	8.09186	8.09186
OCP	d-HCH	delta-hexachlorocyclohexane	319-86-8	JLYXXMFPNIAWKQ-GPIVLXJGSA-N	8.09	
OCP	o,p'-DDE	o,p’-dichlorodiphenyldichloroethylene	3424-82-6	ZDYJWDIWLRZXDB-UHFFFAOYSA-N	9.44	
OCP	p,p'-DDE	p,p'-dichlorodiphenyldichloroethylene	72-55-9	UCNVFOCBFJOQAL-UHFFFAOYSA-N	9.44218	9.44218
OCP	o,p'-DDD	o,p'-dichlorodiphenyldichloroethane	53-19-0	JWBOIMRXGHLCPP-UHFFFAOYSA-N	10.0	
OCP	p,p'-DDD	p,p'-dichlorodiphenyldichloroethane	72-54-8	AHJKRLASYNVKDZ-UHFFFAOYSA-N	10.0	

Compound class	Abbreviation	Name	CAS Number	InChIKey	$logK_{OA}$ (OPERA)[1]	Used $logK_{OA}$[2]
OCP	o,p'-DDT	o,p'-dichlorodiphenyltrichloroethane	789-02-6	CVUGPAFCQJIYDT-UHFFFAOYSA-N	9.57	
OCP	p,p'-DDT	p,p'-dichlorodiphenyltrichloroethane	50-29-3	YVGGHNCTFXOJCH-UHFFFAOYSA-N	9.57	
PBDE	BDE-28	2,4,4'-Tribromodiphenyl ether	41318-75-6	UPNBETHEXPIWQX-UHFFFAOYSA-N	9.45	
PBDE	BDE-47	2,2',4,4'-Tetrabromodiphenyl ether	5436-43-1	XYBSIYMGXVUVGY-UHFFFAOYSA-N	10.5288	10.5288
PBDE	BDE-66	2,3',4,4'-Tetrabromodiphenyl ether	189084-61-5	DHUMTYRHKMCVAG-UHFFFAOYSA-N	10.5	
PBDE	BDE-85	2,2',3,4,4'-pentabromodiphenyl ether	182346-21-0	DMLQSUZPTTUUDP-UHFFFAOYSA-N	11.7	
PBDE	BDE-99	2,2',4,4',5-Pentabromodiphenyl ether	60348-60-9	WHPVYXDFIXRKLN-UHFFFAOYSA-N	11.3471	11.3471
PBDE	BDE-100	2,2',4,4',6-Pentabromodiphenyl ether	189084-64-8	NSKIRYMHNFTRLR-UHFFFAOYSA-N	11.5401	11.5401
PBDE	BDE-153	2,2',4,4',5,5'-hexabromodiphenyl ether	68631-49-2	RZXIRSKYBISPGF-UHFFFAOYSA-N	11.7	
PBDE	BDE-154	2,2',4,4',5,6'-hexabromodiphenyl ether	207122-15-4	VHNPZYZQKWIWOD-UHFFFAOYSA-N	11.7	
PBDE	BDE-183	2,2',3,4,4',5',6-heptabromodiphenyl ether	207122-16-5	ILPSCQCLBHQUEM-UHFFFAOYSA-N	11.7	
PBDE	BDE-209	2,2',3,3',4,4',5,5',6,6'-Decabromodiphenyl ether	1163-19-5	WHHGLZMJPXIBIX-UHFFFAOYSA-N	11.677	14.44[3]
HBCDD	a-HBCDD	beta-Hexabromocyclododecane	134237-51-7	DEIGXXQKDWULML-UFVWWTPHSA-N	11.6814	10.79
HBCDD	b-HBCDD	gamma-Hexabromocyclododecane	134237-52-8	DEIGXXQKDWULML-MOCCIAMBSA-N	11.6814	10.5
HBCDD	g-HBCDD	α-Hexabromocyclododecane	134237-50-6	DEIGXXQKDWULML-PQTSNVLCSA-N	11.6814	9.62

Compound class	Abbreviation	Name	CAS Number	InChIKey	$logK_{OA}$ (OPERA)[1]	Used $logK_{OA}$[2]
NHFR	TBCO	1,2,5,6-Tetrabromocyclooctane	3194-57-8	RZLXIANUDLLFHN-UHFFFAOYSA-N	8.42	
NHFR	PBBZ	Pentabromobenzene	608-90-2	LLVVSBBXENOOQY-UHFFFAOYSA-N	7.92662	7.92662
NHFR	PBEB	Pentabromoethylbenzene	85-22-3	FIAXCDIQXHJNIX-UHFFFAOYSA-N	8.83	
NHFR	TBX	2,3,5,6-tetrabromo-p-xylene	23488-38-2	RXKOKVQKECXYOT-UHFFFAOYSA-N	8.00	
NHFR	DBE-DBCH	1,2-Dibromo-4-(1,2-dibromoethyl)cyclohexane	3322-93-8	PQRRSJBLKOPVJV-UHFFFAOYSA-N	8.42	8.42433
NHFR	TBP-AE	allyl-2,4,6-tribromophenyl ether	3278-89-5	RZLLIOPGUFOWOD-UHFFFAOYSA-N	7.81	
NHFR	BATE	2-Bromoallyl 2,4,6-tribromophenyl ether	99717-56-3	RLPZXGWCSHFKJI-UHFFFAOYSA-N	8.91436	8.91436
NHFR	PBT	Pentabromotoluene	87-83-2	OZHJEQVYCBTHJT-UHFFFAOYSA-N	8.95373	8.95373
NHFR	PBB-Acr	Pentabromobenzyl acrylate	59447-55-1	GRKDVZMVHOLESV-UHFFFAOYSA-N	10.6	
NHFR	HBB	Hexabromobenzene	87-82-1	CAYGQBVSOZLICD-UHFFFAOYSA-N	9.25573	9.25573
NHFR	TBCT	1,2,3,4-Tetrabromo-5-chloro-6-methylbenzene	39569-21-6	WMXWTOJJASZOCL-UHFFFAOYSA-N	8.21	
NHFR	TBP-DBPE	2-3-dibromopropyl-2,4,6-tribromophenyl ether	35109-60-5	QXWYPAKUEHGJSG-UHFFFAOYSA-N	9.81984	9.81984
NHFR	EH-TBB	2-Ethylhexyl 2,3,4,5-tetrabromobenzoate	183658-27-7	HVDXCGSGEQKWGB-UHFFFAOYSA-N	11.5737	12.34[4]
NHFR	DBDPE	decabromodiphenyl ethane	84852-53-9	BZQKBFHEWDPQHD-UHFFFAOYSA-N	11.6758	14.45[7]
NHFR	BEH-TEBP	Bis(2-ethylhexyl) tetrabromophthalate	26040-51-7	UUEDINPOVKWVAZ-UHFFFAOYSA-N	11.6775	15.11[6]

Compound class	Abbreviation	Name	CAS Number	InChIKey	$logK_{OA}$ (OPERA)[1]	Used $logK_{OA}$[2]
NHFR	BTBPE	1,2-Bis(2,4,6-tribromophenoxy)ethane	37853-59-1	YATIGPZCMOYEGE-UHFFFAOYSA-N	11.6856	15.67[4]
NHFR	DBHCTD	hexachlorocyclopentadienyl-dibromocyclooctane	51936-55-1	XRFONNJUMOCNHA-UHFFFAOYSA-N	11.8	
NHFR	DDC-CO	Dechlorane Plus	13560-89-9	UGQQAJOWXNCOPY-UHFFFAOYSA-N	11.7	
NHFR	DDC-CO-MA	Dechlorane Plus Monoadduct	10297-21-9	NA	NA	
OPE	TiBP	Triisobutyl phosphate	126-71-6	HRKAMJBPFPHCSD-UHFFFAOYSA-N	7.38102	7.38102
OPE	TnBP	Tributyl phosphate	126-73-8	STCOOQWBFONSKY-UHFFFAOYSA-N	7.877	7.877
OPE	TCEP	Tris(2-chloroethyl) phosphate	115-96-8	HQUQLFOMPYWACS-UHFFFAOYSA-N	8.41392	8.41392
OPE	TCIPP	Tris(2-chloroisopropyl)phosphate	13674-84-5	KVMPUXDNESXNOH-UHFFFAOYSA-N	8.84716	8.84716
OPE	TDCIPP	Tris(1,3-dichloro-2-propyl)phosphate	13674-87-8	ASLWPAWFJZFCKF-UHFFFAOYSA-N	10.3	
OPE	EHDPP	2-Ethylhexyl diphenyl phosphate	1241-94-7	CGSLYBDCEGBZCG-UHFFFAOYSA-N	11.7254	8.92 [4]
OPE	DBPP	Dibutyl phenyl phosphate	2528-36-1	YICSVBJRVMLQNS-UHFFFAOYSA-N	9.44261	9.44261
OPE	BDPP	Butyl diphenyl phosphate	2752-95-6	DIBUFQMCUZYQKN-UHFFFAOYSA-N	9.75038	9.75038
OPE	TPHP	Triphenyl phosphate	115-86-6	XZZNDPSIHUTMOC-UHFFFAOYSA-N	10.7977	10.7977
OPE	TPrP	tripropyl phosphate	513-08-6	RXPQRKFMDQNODS-UHFFFAOYSA-N	7.26	
OPE	TPeP	Tripentyl phosphate	2528-38-3	QJAVUVZBMMXBRO-UHFFFAOYSA-N	9.37	
OPE	TEHP	Tris(2-ethylhexyl) phosphate	78-42-2	GTVWRXDRKAHEAD-UHFFFAOYSA-N	11.7	

Compound class	Abbreviation	Name	CAS Number	InChIKey	$logK_{OA}$ (OPERA)[1]	Used $logK_{OA}$[2]
OPE	TIPPP	Tris[2-(propan-2-yl)phenyl] phosphate	64532-95-2	LIPMRGQQBZJCTM-UHFFFAOYSA-N	11.6806	11.6806
OPE	TMTP	Phosphoric acid, tris(3-methylphenyl) ester	563-04-2	RMLPZKRPSQVRAB-UHFFFAOYSA-N	11.7031	12.0 [4]
OPE	TOTP	tri-o-cresyl phosphate	78-30-8	YSMRWXYRXBRSND-UHFFFAOYSA-N	11.7	
OPE	TPTP	tri-p-cresyl phosphate	78-32-0	BOSMZFBHAYFUBJ-UHFFFAOYSA-N	11.7	
OPE	TDMPP	Tris(dimethylphenyl) phosphate	25653-16-1	LLPMAOBOEQFPRE-UHFFFAOYSA-N	11.7	
OPE	TBOEP	Tris(2-butoxyethyl) phosphate	78-51-3	WTLBZVNBAKMVDP-UHFFFAOYSA-N	11.7266	13.1 [5]
PAH	NAP	Naphthalene	91-20-3	UFWIBTONFRDIAS-UHFFFAOYSA-N	5.16869	5.16869
PAH	BIP	Biphenyl	92-52-4	ZUOUZKKEUPVFJK-UHFFFAOYSA-N	6.1403	6.1403
PAH	ACE	Acenaphthene	83-32-9	CWRYPZZKDGJXCA-UHFFFAOYSA-N	6.32789	6.32789
PAH	ACY	Acenaphthylene	208-96-8	HXGDTGSAIMULJN-UHFFFAOYSA-N	6.56164	6.56164
PAH	FLU	Fluorene	86-73-7	NIHNNTQXNPWCJQ-UHFFFAOYSA-N	6.8357	6.8357
PAH	ANT	Anthracene	120-12-7	MWPLVEDNUUSJAV-UHFFFAOYSA-N	7.55002	7.55002
PAH	PHE	Phenanthrene	85-01-8	YNPNZTXNASCQKK-UHFFFAOYSA-N	7.55002	7.55002
PAH	BbFLU	11H-Benzo[b]fluorene	243-17-4	HAPOJKSPCGLOOD-UHFFFAOYSA-N	8.51962	8.51962
PAH	RET	Retene	483-65-8	NXLOLUFNDSBYTP-UHFFFAOYSA-N	8.53031	8.53031

Compound class	Abbreviation	Name	CAS Number	InChIKey	$logK_{OA}$ (OPERA)[1]	Used $logK_{OA}$[2]
PAH	BkF	Benzo[k]fluoranthene	207-08-9	HAXBIWFMXWRORI-UHFFFAOYSA-N	9.38	
PAH	BjF	Benzo[j]fluoranthene	205-82-3	KHNYNFUTFKJLDD-UHFFFAOYSA-N	10.3435	10.3435
PAH	BBF	Benzo[b]fluoranthene	205-99-2	FTOVXSOBNPWTSH-UHFFFAOYSA-N	8.63832	8.63832
PAH	PYR	Pyrene	129-00-0	BBEAQIROQSPTKN-UHFFFAOYSA-N	8.855	8.855
PAH	FLA	Fluoranthene	206-44-0	GVEPBJHOBDJJJI-UHFFFAOYSA-N	8.855	8.855
PAH	BNT	Benzo[b]naphtho[2,1-d]thiophene	239-35-0	YEUHHUCOSQOCIX-UHFFFAOYSA-N	8.8607	8.8607
PAH	BAA	Benz[a]anthracene	56-55-3	DXBHBZVCASKNBY-UHFFFAOYSA-N	9.37103	9.37103
PAH	CHR	Chrysene	218-01-9	WDECIBYCCFPHNR-UHFFFAOYSA-N	9.37103	9.37103
PAH	TPY	Triphenylene	217-59-4	SLGBZMMZGDRARJ-UHFFFAOYSA-N	9.37103	9.37103
PAH	BKF	Benzo[k]fluoranthene	207-08-9	HAXBIWFMXWRORI-UHFFFAOYSA-N	9.384	9.384
PAH	CPD	Cyclopenta[cd]pyrene	27208-37-3	BZCXQYVNASLLQO-UHFFFAOYSA-N	9.63083	9.63083
PAH	BghiF	Benzo[ghi]fluoranthene	203-12-3	YEIHPPOCKIHUQJ-UHFFFAOYSA-N	9.92031	9.92031
PAH	BaP	Benzo[a]pyrene	50-32-8	FMMWHPNWAFZXNH-UHFFFAOYSA-N	9.61	
PAH	BeP	Benzo[e]pyrene	192-97-2	TXVHTIQJNYSSKO-UHFFFAOYSA-N	10.3435	10.3435
PAH	DBA	Dibenzo[a,h]anthrancene	53-70-3	LHRCREOYAASXPZ-UHFFFAOYSA-N	11.7	
PAH	IDP	Indeno[1,2,3-cd]pyrene	193-39-5	SXQBHARYMNFBPS-UHFFFAOYSA-N	11.7243	11.7243

Compound class	**Abbreviation**	**Name**	**CAS Number**	**InChIKey**	**$logK_{OA}$ (OPERA)[1]**	**Used $logK_{OA}$[2]**
PAH	BghiP	Benzo[g,h,i]perylene	191-24-2	GYFAGKUZYNFMBN-UHFFFAOYSA-N	11.7243	11.97[4]
PAH	ANTA	Anthanthrene	191-26-4	YFIJJNAKSZUOLT-UHFFFAOYSA-N	11.7	
PAH	COR	Coronene	191-07-1	VPUGDVKSAQVFFS-UHFFFAOYSA-N	11.7	

[1]Predicted by US EPA OPERA model (Mansouri et al., 2018)

[2]The upper boundary based on the $logK_{OA}$ values obtained from the US EPA OPERA model had a maximum of $logK_{OA}$=11.7 for multiple compounds: DBDPE, BDE-209, BEH-TEBP, TIPPP, a-, b- and g-HBCDD, BTBPE, TmTP, IDP, BghiP, EHDPP, TBOEP. This does not reflect the accepted range of octanol-air partitioning coefficients for these compounds, thus, the OPERA values were replaced with specific literature values for these high molecular weight compounds, where indicated.

[3](Environment Canada, 2004)

[4](US EPA, 2023)

[5](Chupeau et al., 2020)

[6](Swedish Chemicals Agency, 2020)

[7](Environment Canada & Health Canada, 2016)

Supplementary Text 1. Instrumental methods

PCBs and OCPs were analyzed via GCMS/MS (Agilent 7890A coupled to Agilent 7000), equipped with a 60 m Restek HT8 column. MS was operated in EI+ mode, at least two transitions were recorded for each compound. Injection was splitless 3 µL at 280°C, with He as the carrier gas. The GC temperature programme was 80°C with a 1.5 min hold, then 40°C min-1 to 200°C, 18 min hold, followed by 5°C min-1 to 305°C

NFRs and PBDEs were analysed via gas chromatography-high resolution mass spectrometry (GC-HRMS) using an Agilent 7890A GC equipped with a 15 m Restek RTX1614 column (with 60 cm retention gap) coupled to a Waters Micromass AutoSpec Premier mass spectrometer. The MS was operated in positive electron impact ionization mode (EI+) using selected ion monitoring (SIM) at a resolution >10000. Injection was splitless 3 µl at 280 °C for PBDEs, with He as the carrier gas at 1 ml/min. The GC temperature program was 80 °C with a 1 min hold, then 20 °C/min to 250 °C, followed by 1.5 °C/min to 260 °C with a 2 min hold and 25 °C/min to 320 °C with a 4.5 min hold. For NFRs Injection was splitless 2 µl at 250 °C, with He as the carrier gas at 1.2 ml/min. The GC temperature program was 80 °C with a 1 min hold, then 30 °C/min to 140 °C, followed by 4°C/min to 175 °C and 8°C/min to 270 and 15 °C/min to 325 °C with a 5 min hold.

PAHs were analyzed using a GC coupled to a low resolution mass selective detector (MS) (Agilent 7890A - Agilent 7000B), with a 60 m x 0.25 mm x 0.25 µm J&W Scientific DB–5MSUI column in EI+ mode. Injection was splitless 1 µL at 280°C, with He as the carrier gas. The GC temperature programme was 80°C with a 1 min hold, then 15°C·min-1 to 180°C, followed by 5°C·min-1 to 310°C with a 20 min hold.

OPEs were analysed using an Agilent 7890A GC equipped with a 15 m Restek RTX1614 column (with 60 cm retention gap) coupled to a Waters APGC XEVO TQ-S tandem mass spectrometer (MS/MS). The MS was operated in positive atmospheric pressure ionization mode (APGC+) using multiple reaction monitoring mode (MRM). At least two transitions were recorded for each compound. Additional parameters were set as follows: source temperature 150 °C, cone gas flow 160 L/Hr, auxiliary gas flow 220 L/Hr. Injection was splitless 1 µL at 250 °C, with He as the carrier gas at 1.2 mL·min^{-1}. The GC temperature program was 80 °C with a 1 min hold, then 30 °C·min-1 to 140 °C, followed by 4 °C·min-1 to 175 °C, then 8 °C·min-1 to 270 °C and 15 °C·min-1 to 325 °C with a 7 min hold. Makeup gas pressure was 60 psi and transfer line temperature was set to 300 °C.

HBCDDs were analyzed after exchanging solvent to acetonitrile by liquid chromatography electrospray ionization mass spectrometry using HPLC apparatus Agilent 1290 series (Agilent Technologies, Waldbronn, Germany) consisting of a vacuum degasser, a binary pump, an thermostated autosampler (10°C), and a thermostated column compartment kept at 30°C. The column was Phenomenex Luna C-18 endcapped (3 µm) 100 x 2 mm i.d., equipped with Phenomenex SecureGuard C18 guard column (Phenomenex, Torrance, CA, USA). The mobile phase consisted of 1 mM ammonium acetate in water, pH 4 (A) and 1 mM ammonium acetate in acetonitrile (B). The binary pump gradient was non-linear (increase from 50% B at 0 min to 90% B at 6 min, then 90% B for 8 min and 5 min column equilibration to initial conditions (50% B)); the flow rate was 0.25 mL/min. 10 μL of individual sample was injected for the analyses. The mass spectrometer was an AB Sciex Qtrap 5500 (AB Sciex, Concord, ON, Canada) with electrospray ionization (ESI). Ions were detected in the negative mode. The ionization parameters were as follows: capillary voltage, -4 kV; desolvation temperature, 450°C; Curtain gas 15 psi, Gas1 40 psi, Gas2 40 psi.

Supplementary Table 3. Method detection limits and detection frequencies of individual target compounds. Compounds with >50% detection frequency were used for further calibration

	PAS PUF	AAS PUF	AAS QFF	Detection
	pg/PAS	pg/m3	pg/m3	frequency (%)
PCB 9	0.037	0.001	0.00003	63%
PCB 11	0.924	0.318	0.00025	100%
PCB 28	0.020	0.037	0.00007	100%
PCB 52	0.020	0.018	0.00007	100%
PCB 101	0.070	0.007	0.00023	81%
PCB 118	0.060	0.001	0.00020	14%
PCB 153	0.090	0.004	0.00030	67%
PCB 138	0.100	0.002	0.00033	19%
PCB 180	0.090	0.001	0.00030	17%
PeCB	0.040	0.010	0.00013	92%
HCB	0.030	0.058	0.00010	99%
a-HCH	0.040	0.019	0.00013	90%
g-HCH	0.050	0.046	0.00045	91%
o,p'-DDE	0.030	0.002	0.00010	16%
p,p'-DDE	0.102	0.024	0.00010	99%
o,p'-DDD	0.030	0.00041	0.00010	7%
p,p'-DDD	0.020	0.001	0.00007	18%
o,p'-DDT	0.080	0.003	0.00027	31%
p,p'DDT	0.040	0.001	0.00013	48%
BDE 28	4.95 (3-63)	0.01-0.38	0.01-0.38	3%
BDE 47	1.4	0.0388	0.01-0.29	91%
BDE 66	6.89 (1-168)	0.01-0.50	0.01-0.50	7%
BDE 100	0.39	0.01-0.67	0.01-0.67	68%
BDE 99	0.898	0.142	0.01-2.39	85%
BDE 85	7.75 (3-163)	0.01-1.89	0.01-1.89	0%
BDE 154	9.08 (4-114)	0.02-1.78	0.02-1.78	0%
BDE 153	12.3 (7-139)	0.02-1.39	0.02-1.39	0%
BDE 183	2.68	0.02-1.94	0.02-1.94	43%
BDE 209	142	12.2	0.933	81%
Naphthalene	108000	530	58.3	93%
Acenaphthylene	4300	10.1	3.4	99%
Acenaphthene	10900	27.1	3.18	90%
Fluorene	15800	61.3	11.5	93%
Phenanthrene	23900	150	30.8	99%
Anthracene	1090	12.7	2.18	99%
Fluoranthene	13700	375	14.5	90%
Pyrene	6660	350	5.25	98%
Benzo-a-anthracene	342	190	1.8	89%

	PAS PUF	AAS PUF	AAS QFF	Detection frequency (%)
	pg/PAS	pg/m3	pg/m3	
Chrysene	889	269	3	80%
Benzo-b-fluoranthene	876	429	1.85	37%
Benzo-k-fluoranthen	257	264	0.6	67%
Benzo-a-pyrene	116	184	0.1	48%
Indeno-123cd-pyrene	74.8	147	0.1	71%
Dibenzo(ah)anthracene	34.3	0.2	0.1	37%
Benzo-ghi-perylene	116	647	0.2	75%
Biphenyl	58050	341	29.2	91%
Retene	1290	27.9	5	98%
Benzo-b-fluorene	482	55.1	0.6	80%
Benzonapthothiophene	230	18.1	0.2	84%
Benzo-ghi-fluoranthene	621	134	1.45	76%
Cyclopenta-cd-pyrene	191	470	0.2	90%
Triphenylene	700	70.7	1.03	68%
Benzo-j-fluoranthene	271	314	0.3	63%
Benzo-e-pyrene	159	464	0.3	60%
Perylene	97.8	31.8	0.3	12%
Dibenzo(ac)anthracene	45.2	0.2	0.2	26%
Anthanthrene	94.9	41.6	0.300	9%
Coronene	168	47.2	0.600	9%
TPrP	1.00	0.00333	0.00333	0%
TiBP	4200	37.3	45.4	99%
TnBP	45600	211	166	88%
TCEP	5660	43.3	10.6	99%
TCIPP	59900	687	83.6	99%
DBPP	1.00	0.00333	0.00333	99%
TPeP	0.100	2.08	0.00033	14%
BDPP	1.00	0.00333	0.00333	79%
TDCIPP	56000	771	8.45	9%
TBEP	6840	78.6	0.160	92%
TPhP	18300	97.8	10.6	80%
EHDPP	1750	17.2	2.31	92%
TEHP	12930	6.90	1.58	21%
ToTP	189	1.19	0.437	29%
TmTP	1.00	0.00333	0.00333	92%
TpTP	1.00	0.00333	0.00333	8%
TIPPP	123	0.464	0.100	64%
TDMPP	0.1	0.000333	0.000333	0%
TBP-AE	0.177	0.000589	0.000589	57%
DBE-DBCH	1.36	0.767	0.00454	91%
TBX	0.165	0.000551	0.000551	0%
BATE	0.153	0.00051	0.000510	91%
TBCO	2.49	0.00830	0.00830	0%
PBBZ	0.161	0.155	0.000537	99%
TBCT	0.141	0.000469	0.000469	48%

	PAS PUF	AAS PUF	AAS QFF	Detection
	pg/PAS	pg/m3	pg/m3	frequency (%)
DDC-CO-MA	1.37	0.004555	0.004555	0%
PBT	0.186	0.00062	0.000620	87%
PBEB	0.191	0.000637	0.000637	9%
TBP-DBPE	13.3	3.86	0.0444	89%
HBB	2.81	10.1	0.00496	98%
PBB-Acr	4.79	0.0159	0.0160	42%
DBHCTD	1.10	0.00366	0.00366	0%
EH-TBB	6.39	1.60	0.0213	74%
BTBPE	14.4	0.223	0.00460	60%
s-DDC-CO	620	10.5	10.8	74%
a-DDC-CO	336	4.037	3.59	74%
BEH-TEBP	11.7	0.433	0.0391	58%
DBDPE	609	0.657	0.657	71%
a HBCDD	2.5	0.025	0.025	95%
b HBCDD	1	0.01	0.010	92%
g HBCDD	2.5	0.025	0.025	92%
d HBCDD	2.5	0.025	0.025	0%

Supplementary Table 4. Data sources identified for literature review, grouped by method of calibration

Reference	Location	Compounds class	Sorbent	PUF size	Housing	Calibration method	Sampling rate value or range (m^3/d)
Kim SK, Shoeib M, Kim KS, Park JE. Indoor and outdoor poly- and perfluoroalkyl substances (PFASs) in Korea determined by passive air sampler. Environ Pollut. 2012;162:144-50. doi: 10.1016/j.envpol.2011.10.037	Indoor, homes	PFAS	PUF	14 cm x 13.5 mm	Double bowl	AAS calibration	1.2
Herkert NJ , Hornbuckle KC . Effects of room airflow on accurate determination of PUF-PAS sampling rates in the indoor environment. Environ Sci Process Impacts. 2018;20(5):757-766. doi: 10.1039/c8em00082d.	Indoor, office	PCBs	PUF	13.97 cm x 12.7 mm	Double bowl	AAS calibration	1.32
Wilford BH, Harner T, Zhu J, Shoeib M, Jones KC. Passive sampling survey of polybrominated diphenyl ether flame retardants in indoor and outdoor air in Ottawa, Canada: implications for sources and exposure. Environ Sci Technol. 2004; 38(20):5312-8. doi: 10.1021/es049260x.	Indoors, offices	PBDEs	PUF	14 cm x 13.5 mm	Upper plate	AAS calibration	2.5
Herkert NJ , Hornbuckle KC . Effects of room airflow on accurate determination of PUF-	Indoor, office	PCBs	PUF	13.97 cm x 12.7 mm	Upper bowl	AAS calibration	2.72

Reference	Location	Compounds class	Sorbent	PUF size	Housing	Calibration method	Sampling rate value or range (m^3/d)
PAS sampling rates in the indoor environment. Environ Sci Process Impacts. 2018; 20(5):757-766. doi: 10.1039/c8em00082d.							
Bohlin P, Audy O, Škrdlíková L, Kukučka P, Vojta Š, Přibylová P, Prokeš R, Čupr P, Klánová J. Evaluation and guidelines for using polyurethane foam (PUF) passive air samplers in double-dome chambers to assess semi-volatile organic compounds (SVOCs) in non-industrial indoor environments. Environ Sci Process Impacts. 2014; 16(11):2617-26. doi: 10.1039/c4em00305e.	Indoor, laboratory	PCBs, OCPs, PBDEs, NHFRs, PAHs, PCDD/Fs	PUF	15 cm x 15 mm	Double bowl	AAS calibration	0.03-5.5
Feng YX, Feng NX, Zeng LJ, Chen X, Xiang L, Li YW, Cai QY, Mo CH. Occurrence and human health risks of phthalates in indoor air of laboratories. Sci Total Environ. 2020; 707:135609. doi: 10.1016/j.scitotenv.2019.135609.	Indoor, laboratory	PAEs	PUF	14 cm x 12 mm	Double bowl	AAS calibration	0.124-10.565
Kim, SK., Park, JE. Comparison of two different passive air samplers (PUF-PAS versus SIP-PAS) to determine time-integrated	Indoor, homes	PFAS	PUF	14 cm x 13.5 mm	Double bowl	AAS calibration	0.19-1.32

Reference	Location	Compounds class	Sorbent	PUF size	Housing	Calibration method	Sampling rate value or range (m^3/d)
average air concentration of volatile hydrophobic organic pollutants. Ocean Sci. J. 2014; 49:137–150 doi: 10.1007/s12601-014-0014-9							
Meng, ZY; Wang, LX; Cao, BK; Huang, ZS; Liu, F; Zhang, JP. Indoor airborne phthalates in university campuses and exposure assessment. 2020; 180:107002. doi: 10.1016/j.buildenv.2020.107002	Indoor, university buildings	PAEs	PUF	14 cm x 12.7 mm	No housing, paper filter to block dust	AAS calibration	0.40-0.97
Bohlin P, Jones KC, Strandberg B. Field evaluation of polyurethane foam passive air samplers to assess airborne PAHs in occupational environments. Environ Sci Technol. 2010;44(2):749-54. doi: 10.1021/es902318g.	Indoor, industrial	PAHs	PUF	14 cm x 10 mm	Upper plate	AAS calibration	0.43-16.5
Bohlin P, Jones KC, Strandberg B. Field evaluation of polyurethane foam passive air samplers to assess airborne PAHs in occupational environments. Environ Sci Technol. 2010;44(2):749-54. doi: 10.1021/es902318g.	Indoor, industrial	PAHs	PUF	14 cm x 10 mm	Double bowl	AAS calibration	0.45-14.4

Reference	Location	Compounds class	Sorbent	PUF size	Housing	Calibration method	Sampling rate value or range (m^3/d)
Saini A, Okeme JO, Goosey E, Diamond ML. Calibration of two passive air samplers for monitoring phthalates and brominated flame-retardants in indoor air. Chemosphere. 2015;137:166-73. doi: 10.1016/j.chemosphere.2015.06.099.	Indoor, university buildings	BFRs	PUF	14 cm x 12 mm	Double bowl	AAS calibration	0.6-1.9
Saini A, Okeme JO, Goosey E, Diamond ML. Calibration of two passive air samplers for monitoring phthalates and brominated flame-retardants in indoor air. Chemosphere. 2015;137:166-73. doi: 10.1016/j.chemosphere.2015.06.099.	Indoor, university buildings	BFRs	PUF	14 cm x 12 mm	Upper bowl	AAS calibration	0.6-4.3
Harrad S, Abdallah MA. Calibration of two passive air sampler configurations for monitoring concentrations of hexabromocyclododecanes in indoor air. J Environ Monit. 2008;10(4):527-31. doi: 10.1039/b719638e.	Indoor, offices	HBCDDs	PUF	14 cm x 12 mm	Double bowl	AAS calibration	0.87-0.91
Harrad S, Abdallah MA. Calibration of two passive air sampler configurations for	Indoor, offices	HBCDDs	PUF	14 cm x 12 mm	Upper bowl	AAS calibration	1.38-1.55

Reference	Location	Compounds class	Sorbent	PUF size	Housing	Calibration method	Sampling rate value or range (m^3/d)
monitoring concentrations of hexabromocyclododecanes in indoor air. J Environ Monit. 2008;10(4):527-31. doi: 10.1039/b719638e.							
Shoeib M, Harner T. Characterization and comparison of three passive air samplers for persistent organic pollutants. Environ Sci Technol. 2002;36(19):4142-51. doi: 10.1021/es020635t	Indoor, laboratory	PCBs	PUF	14 cm x 13.5 mm	Mesh case	AAS calibration	1.8-8.3
Dodson RE, Bessonneau V, Udesky JO, Nishioka M, McCauley M, Rudel RA. Passive indoor air sampling for consumer product chemicals: a field evaluation study. J Expo Sci Environ Epidemiol. 2019; 29(1):95-108. doi: 10.1038/s41370-018-0070-9.	Indoor, homes and offices	SVOCs	PUF	13.97 cm x 12.7 mm	Mesh case	AAS calibration	2.11-18.6
Okeme JO, Yang C, Abdollahi A, Dhal S, Harris SA, Jantunen LM, Tsirlin D, Diamond ML. Passive air sampling of flame retardants and plasticizers in Canadian homes using PDMS, XAD-coated PDMS and PUF samplers. Environ Pollut. 2018; 239:109-	Indoor, university buildings	PAEs, FRs	PUF	14 cm x 12 mm	Upper bowl	AAS calibration	2.9-14

Reference	Location	Compounds class	Sorbent	PUF size	Housing	Calibration method	Sampling rate value or range (m^3/d)
117. doi: 10.1016/j.envpol.2018.03.103							
Karaskova, P; Codling, G; Melymuk, L; Klanova, J. A critical assessment of passive air samplers for per- and polyfluoroalkyl substances. Atm. Env. 2018; 185:186-195. doi: 10.1016/j.atmosenv.2018.05.030	Indoor, university buildings	PFAS	PUF	15 cm x 15 mm	Double bowl	AAS calibration	3.32-14.4
Herkert NJ , Hornbuckle KC . Effects of room airflow on accurate determination of PUF-PAS sampling rates in the indoor environment. Environ Sci Process Impacts. 2018 ;20(5):757-766. doi: 10.1039/c8em00082d.	Indoor, office	PCBs	PUF	13.97 cm x 12.7 mm	Double bowl	Computational fluid dynamic model predicted	1.05
Herkert NJ , Hornbuckle KC . Effects of room airflow on accurate determination of PUF-PAS sampling rates in the indoor environment. Environ Sci Process Impacts. 2018 ;20(5):757-766. doi: 10.1039/c8em00082d.	Indoor, office	PCBs	PUF	13.97 cm x 12.7 mm	Upper bowl	Computational fluid dynamic model predicted	2.62
Persoon C, Hornbuckle KC. Calculation of passive sampling rates from both native PCBs and depuration compounds in indoor and outdoor environments. Chemosphere. 2009	Indoor, university buildings	PCBs	PUF	14 cm x 13.5 mm	Double bowl	Experimental/time trend uptake	2.0-3.5

Reference	Location	Compounds class	Sorbent	PUF size	Housing	Calibration method	Sampling rate value or range (m^3/d)
Feb;74(7):917-23. doi: 10.1016/j.chemosphere.2008.10.011.							
Bohlin P, Jones KC, Strandberg B. Field evaluation of polyurethane foam passive air samplers to assess airborne PAHs in occupational environments. Environ Sci Technol. 2010 Jan 15;44(2):749-54. doi: 10.1021/es902318g.	Indoor, industrial	PAHs	PUF	14 cm x 10 mm	Upper plate	Performance reference compound-derived	1-5.1
Persoon C, Hornbuckle KC. Calculation of passive sampling rates from both native PCBs and depuration compounds in indoor and outdoor environments. Chemosphere. 2009;74(7):917-23. doi: 10.1016/j.chemosphere.2008.10.011.	Indoor, university buildings	PCBs	PUF	14 cm x 13.5 mm	Double bowl	Performance reference compound-derived	2.1-2.7
Armstrong JL, Yost MG, Fenske RA. Development of a passive air sampler to measure airborne organophosphorus pesticides and oxygen analogs in an agricultural community. Chemosphere. 2014;111:135-43. doi: 10.1016/j.chemosphere.2014.03.064	Indoor, laboratory chamber	CUPs	PUF	14 cm x 13 mm	No housing (chamber tests)	Performance reference compound-derived	2.25-3.04

Reference	**Location**	**Compounds class**	**Sorbent**	**PUF size**	**Housing**	**Calibration method**	**Sampling rate value or range (m^3/d)**
Anh HQ, Tomioka K, Tue NM, Tuyen LH, Chi NK, Minh TB, Viet PH, Takahashi S. A preliminary investigation of 942 organic micro-pollutants in the atmosphere in waste processing and urban areas, northern Vietnam: Levels, potential sources, and risk assessment. Ecotoxicol Environ Saf. 2019 ;167:354-364. doi: 10.1016/j.ecoenv.2018.10.026.	Semi-open, industrial, waste workshops	SVOCs	PUF	13.6 cm x 13 mm	Double bowl	Extracted from literature	2.5-3.5
Marek RF, Thorne PS, Herkert NJ, Awad AM, Hornbuckle KC. Airborne PCBs and OH-PCBs Inside and Outside Urban and Rural U.S. Schools. Environ Sci Technol. 2017 ;51(14):7853-7860. doi: 10.1021/acs.est.7b01910.	Indoor, schools	PCBs	PUF	14 cm x 13.5 mm	Double bowl	Extracted from literature	0.8
Melymuk L, Bohlin-Nizzetto P, Vojta Š, Krátká M, Kukučka P, Audy O, Přibylová P, Klánová J. Distribution of legacy and emerging semivolatile organic compounds in five indoor matrices in a residential environment. Chemosphere. 2016;153:179-86. doi:	Indoor, home	PCBs	PUF	15 cm x 15 mm	Upper bowl	Extracted from literature	1.4

Reference	Location	Compounds class	Sorbent	PUF size	Housing	Calibration method	Sampling rate value or range (m^3/d)
10.1016/j.chemosphere.2016.03.012.							
Muenhor D, Harrad S, Ali N, Covaci A. Brominated flame retardants (BFRs) in air and dust from electronic waste storage facilities in Thailand. Environ Int. 2010;36(7):690-8. doi: 10.1016/j.envint.2010.05.002.	Indoor, e-waste storage facilities	BFRs	PUF	14 cm x 12 mm	Double bowl	Extracted from literature	1.66
Ali N, Ali L, Mehdi T, Dirtu AC, Al-Shammari F, Neels H, Covaci A. Levels and profiles of organochlorines and flame retardants in car and house dust from Kuwait and Pakistan: implication for human exposure via dust ingestion. Environ Int. 2013;55:62-70. doi: 10.1016/j.envint.2013.02.001.	Indoor, homes and offices	PBDEs	PUF	14 cm x 12 mm	Double bowl	Extracted from literature	2.5
Bohlin, P., Jones, K.C., Tovalin, H., Strandberg, B. Observations on persistent organic pollutants in indoor and outdoor air using passive polyurethane foam samplers Atm. Env. 2008; 42. doi: 10.1016/j.atmosenv.2008.07.012	Indoor, homes	PAHs	PUF	14 cm x 12 mm	Upper plate	Extracted from literature	2.5
Villanueva, F; Sevilla, G; Lara, S; Martin, P; Salgado, S; Albaladejo, J; Cabanas, B. Application of gas	Indoor, homes	PAHs	PUF	14 cm x 12 mm	Double bowl	Extracted from literature	0.4-4.0

Reference	Location	Compounds class	Sorbent	PUF size	Housing	Calibration method	Sampling rate value or range (m^3/d)
chromatography coupled with tandem mass spectrometry for the assessment of PAH levels in non industrial indoor air. Microchem. J. 2018; 142:117-125. doi: 10.1016/j.microc.2018.06.021							
Harrad S, Hazrati S, Ibarra C. Concentrations of polychlorinated biphenyls in indoor air and polybrominated diphenyl ethers in indoor air and dust in Birmingham, United Kingdom: implications for human exposure. Environ Sci Technol. 2006 Aug 1;40(15):4633-8. doi: 10.1021/es0609147	Indoor, homes, offices, cars, public spaces	PCBs, PBDEs	PUF	14 cm x 12 mm	Double bowl	Extracted from literature	0.70-1.9
Hazrati, S; Harrad, S; Alighadri, M; Sadeghi, H; Mokhtari, A; Gharari, N; Rahimzadeh, S. Passive air sampling survey of polybrominated diphenyl ether in private cars: implications for sources and human exposure. Iran. J. Environ. Health. Sci. Eng., 2010; 7(2):157-164	Indoor, cars	PBDEs	PUF	14 cm x 12 mm	Double bowl	Extracted from literature	1.12-1.94
Zhang X, Diamond ML, Robson M, Harrad S. Sources, emissions, and fate of polybrominated diphenyl ethers and	Indoors, homes and offices	PBDEs	PUF	14 cm x 12 mm	Double bowl	Extracted from literature	1.12-1.94

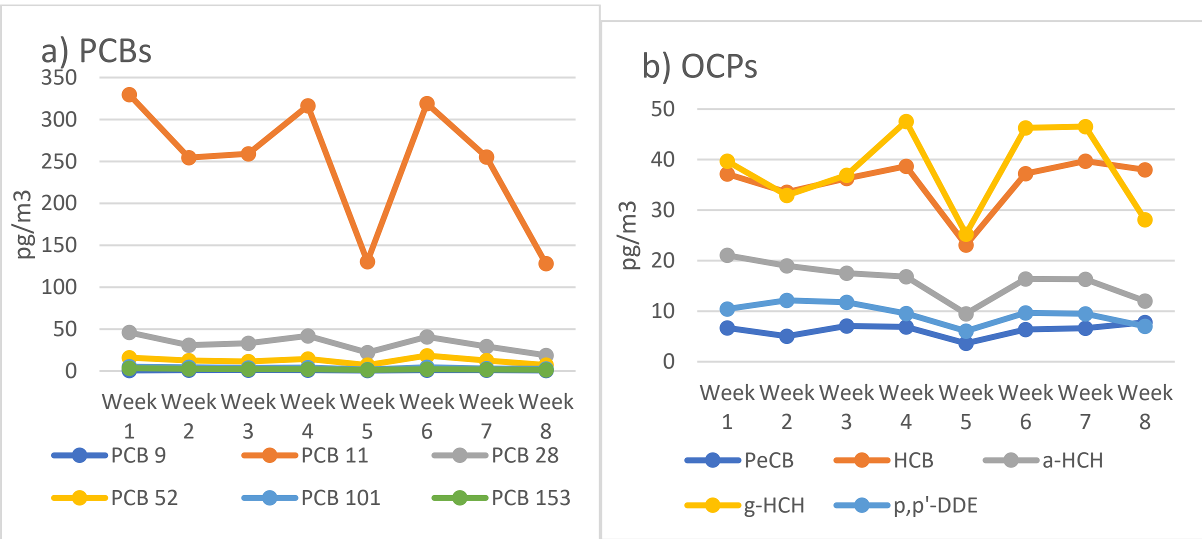
Reference	Location	Compounds class	Sorbent	PUF size	Housing	Calibration method	Sampling rate value or range (m^3/d)
polychlorinated biphenyls indoors in Toronto, Canada. Environ Sci Technol. 2011 Apr 15;45(8):3268-74. doi: 10.1021/es102767g.							
Khan MU, Besis A, Li J, Zhang G, Malik RN. New insight into the distribution pattern, levels, and risk diagnosis of FRs in indoor and outdoor air at low- and high-altitude zones of Pakistan: Implications for sources and exposure. Chemosphere. 2017;184:1372-1387. doi: 10.1016/j.chemosphere.2017.06.056	Indoor, homes, workplaces	FRs	PUF	14 cm x 13.5 mm	Double bowl	Extracted from literature	Not specified
Adesina, OA; Ojesola, FF; Olowolafe, TI; Igbafe, A. Assessment of PAHs Emissions from Domestic Cooking Fuels on Indoor Air in Nigeria. JST: Engineering and Technology for Sustainable Development. 2022;32(5):070-078	Indoor, workplaces	PAHs	PUF	15 cm x 8 mm	Upper plate	GAPS template with default sampling rate of 2 m3/d	Not specified
Adesina OA, Nwogu AS, Lala MA, Adeyemo AT, Sonibare JA. Concentrations of polychlorinated biphenyl in indoor environment of public bars and its health implications. Environ Monit	Indoor, bars	PCBs	PUF	14 cm x 13.5 mm	Upper bowl	Unclear, with reference to GAPS template, but not further specified	Not specified

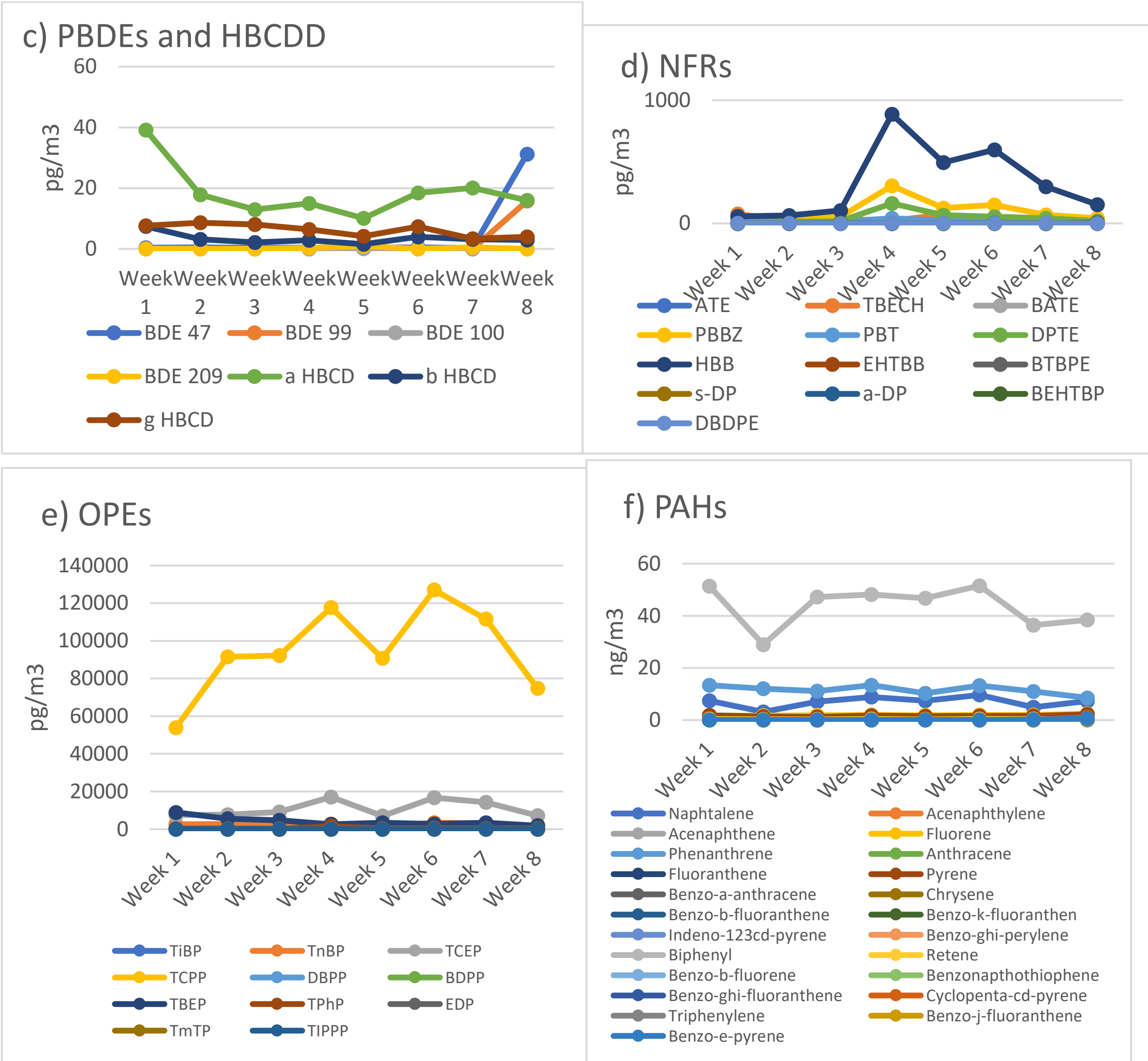
Reference	Location	Compounds class	Sorbent	PUF size	Housing	Calibration method	Sampling rate value or range (m^3/d)
Assess. 2021 Aug 28;193(9):605. doi: 10.1007/s10661-021-09405-3.							
Yu S, Gao Y, Zhu X, Yu H, Zhang Y, Chen J. Gas/particle partitioning of short and medium chain chlorinated paraffins from a CP production plant using passive air sampler and occupational exposure assessment. Sci Total Environ. 2023 Feb 1;858(Pt 1):159875. doi: 10.1016/j.scitotenv.2022.159875.	Indoor, industrial	CPs	PUF with GFF	14 cm x 12 mm	No housing info given	Not specified	Not specified
Adesina OA, Nwogu AS, Sonibare JA. Indoor levels of polycyclic aromatic hydrocarbons (PAHs) from environment tobacco smoke of public bars. Ecotoxicol Environ Saf. 2021 Jan 15;208:111604. doi: 10.1016/j.ecoenv.2020.111604. Epub 2020 Nov 13.	Indoor, bars	PAHs	PUF	14 cm x 13.5 mm	Upper bowl or plate	Not specified	Not specified

Supplementary Table 5. Bulk air concentration measured by AAS and particle-bound fraction

		Average bulk conc.	Particle fraction (%)
PCBs (pg/m^3)	PCB 9	0.902	6.2%
	PCB 11	249	6.0%
	PCB 28	32.80	4.8%
	PCB 52	12.4	5.4%
	PCB 101	3.63	7.6%
	PCB 153	2.10	9.7%
OCPs (pg/m^3)	PeCB	6.27	8.6%
	HCB	35.5	6.3%
	a-HCH	16.1	13%
	g-HCH	37.9	12%
	p,p'-DDE	9.53	6.4%
PBDEs (pg/m^3)	BDE 47	4.24	8%
	BDE 99	2.03	72%
	BDE 100	0.0236	0%
	BDE 209	0.208	100%
HBCDDs (pg/m^3)	a HBCDD	18.7	90%
	b HBCDD	3.38	90%
	g HBCDD	6.19	84%
NFRs (pg/m^3)	TBP-AE	ND	NA
	DBE-DBCH	35.6	0%
	BATE	3.14	0%
	PBBZ	104	0%
	PBT	20.2	0%
	TBP-DBPE	48.8	3%
	HBB	332	2%
	EH-TBB	0.573	92%
	BTBPE	0.0478	100%
	s-DDC-CO	0.979	100%
	a-DDC-CO	0.904	100%
	BEH-TEBP	0.797	0%
	DBDPE	0.512	0%
OPEs (ng/m^3)	TiBP	977	9%
	TnBP	2450	17%
	TCEP	10850	12%
	TCIPP	94900	33%
	DBPP	749	20%
	BDPP	19.3	41%
	TBEP	4150	94%
	TPhP	554	67%
	EHDPP	263	94%
	TmTP	4.80	98%
	TIPPP	4.77	93%

PAHs (ng/m^3)	Naphthalene	6.98	1%
	Acenaphthylene	0.226	3%
	Acenaphthene	0.618	1%
	Fluorene	1.92	1%
	Phenanthrene	11.6	1%
	Anthracene	0.647	1%
	Fluoranthene	1.20	11%
	Pyrene	1.64	9%
	Benzo-a-anthracene	0.108	98%
	Chrysene	0.104	100%
	Benzo-b-fluoranthene	0.182	100%
	Benzo-k-fluoranthene	0.0814	100%
	Indeno-123cd-pyrene	0.125	100%
	Benzo-ghi-perylene	0.199	100%
	Biphenyl	43.6	0%
	Retene	0.349	4%
	Benzo-b-fluorene	0.0408	93%
	Benzonapthothiophene	0.0154	64%
	Benzo-ghi-fluoranthene	0.0591	100%
	Cyclopenta-cd-pyrene	0.219	100%
	Triphenylene	0.0297	100%
	Benzo-j-fluoranthene	0.0946	100%
	Benzo-e-pyrene	0.143	100%





Supplementary Figure 1. Ambient indoor air concentrations of target compound groups over time for all compounds with >50% detection frequency.

Supplementary Table 6. Relative standard deviations (%) of the three replicates of each sampler configuration, by compound

Compound	Double bowl (Day 56)	Single bowl (Day 56)	No-bowl (Day 49)
PCB 9	6%	9%	19%
PCB 11	9%	4%	18%
PCB 28	8%	15%	22%
PCB 52	6%	12%	16%
PCB 101	6%	14%	22%
PCB 153	13%	15%	21%
PeCB	5%	9%	26%
HCB	5%	8%	11%
a-HCH	16%	8%	16%
g-HCH	11%	11%	19%
p,p'-DDE	16%	7%	19%

BDE 47	18%	15%	28%
BDE 100	18%	67%	130%
BDE 99	10%	74%	41%
BDE 209	66%	30%	17%
a HBCDD	40%	18%	4%
b HBCDD	39%	14%	7%
g HBCDD	27%	59%	3%
TBP-AE	18%	37%	141%
DBE-DBCH	6%	8%	48%
BATE	12%	12%	25%
PBBZ	8%	15%	17%
PBT	13%	12%	71%
TBP-DBPE	14%	27%	71%
HBB	12%	15%	8%
EH-TBB	65%	28%	70%
BTBPE	48%	14%	21%
s-DDC-CO	62%	38%	79%
a-DDC-CO	77%	17%	48%
BEH-TEBP	95%	58%	71%
DBDPE	123%	137%	NA
TiBP	7%	11%	7%
TnBP	45%	9%	5%
TCEP	9%	13%	14%
TCIPP	24%	5%	25%
DBPP	6%	16%	10%
BDPP	20%	16%	9%
TBOEP	35%	19%	10%
TPhP	28%	10%	10%
EDP	20%	9%	17%
TmTP	34%	17%	9%
TIPPP	29%	11%	15%
Naphthalene	3%	3%	4%
Acenaphthylene	6%	5%	6%
Acenaphthene	4%	7%	9%
Fluorene	3%	1%	4%
Phenanthrene	6%	6%	5%
Anthracene	6%	7%	9%
Fluoranthene	19%	8%	9%
Pyrene	8%	11%	9%
Benzo-a-anthracene	21%	9%	11%
Chrysene	25%	11%	7%
Benzo-b-fluoranthene	16%	22%	20%
Benzo-k-fluoranthene	25%	13%	7%
Indeno-123cd-pyrene	17%	24%	41%
Benzo-ghi-perylene	21%	18%	12%
Biphenyl	4%	6%	7%

Retene	4%	21%	14%
Benzo-b-fluorene	11%	12%	12%
Benzonapthothiophene	33%	12%	12%
Benzo-ghi-fluoranthene	17%	12%	7%
Cyclopenta-cd-pyrene	27%	5%	11%
Triphenylene	19%	14%	6%
Benzo-j-fluoranthene	20%	14%	15%
Benzo-e-pyrene	56%	8%	6%
Minimum	3%	1%	3%
Maximum	123%	137%	141%
Median	17%	12%	14%
Mean	23%	18%	23%
Standard deviation	23%	21%	27%

Supplementary Table 7. Regression results for determination of SR

Cmpd class	Compound	Bowl	Regression		Constant						Slope							SR	Reason for invalid SR
			R^2	Std. Error of the Estimate	B	Std. Error of constant	t	Sig. of constant	95% CI LB of constant	95% CI UB of constant	Slope	Std. Error of slope	Std. slope	t	Sig. of slope	95% LB of slope	95% UB of slope		
NHFR	DBE-DBCH	Double	0.881	10.21	-15.37	4.486	-3.426	0.002	-24.61	-6.131	1.765	0.13	0.939	13.615	<.001	1.498	2.032		At t=0, Veq≠0
OPE	BDPP	Double	0.767	16.57	-29.88	7.332	-4.075	<.001	-45.01	-14.75	1.87	0.21	0.876	8.887	<.001	1.436	2.305		At t=0, Veq≠0
OPE	TCIPP	Double	0.469	26.32	36.32	11.65	3.118	0.005	12.28	60.36	1.54	0.334	0.685	4.607	<.001	0.85	2.231		At t=0, Veq≠0
OPE	TPhP	Double	0.181	11.31	36.12	5.005	7.218	<.001	25.79	46.45	0.331	0.144	0.425	2.301	0.03	0.034	0.627		At t=0, Veq≠0
PAH	IDP	Double	0.19	0.418	1.394	0.187	7.444	<.001	1.008	1.781	-0.013	0.005	-0.436	-2.37	0.026	-0.024	-0.002		At t=0, Veq≠0
PAH	FLU	Double	0.946	8.272	9.954	3.709	2.684	0.013	2.299	17.61	2.17	0.106	0.973	20.492	<.001	1.952	2.389		At t=0, Veq≠0
PAH	BjF	Double	0.263	2.36	6.368	1.058	6.016	<.001	4.183	8.552	-0.088	0.03	-0.513	-2.927	0.007	-0.151	-0.026		At t=0, Veq≠0
PAH	BKF	Double	0.285	2.196	6.25	0.985	6.346	<.001	4.218	8.283	-0.087	0.028	-0.534	-3.095	0.005	-0.145	-0.029		At t=0, Veq≠0
PAH	BBF	Double	0.319	2.546	11.75	1.142	10.29	<.001	9.392	14.11	-0.109	0.033	-0.564	-3.35	0.003	-0.176	-0.042		At t=0, Veq≠0
PAH	ACE	Double	0.795	36.86	57.49	16.53	3.478	0.002	23.37	91.6	4.553	0.472	0.892	9.647	<.001	3.579	5.527		At t=0, Veq≠0
PAH	ACY	Double	0.851	33.42	65.92	14.99	4.399	<.001	34.99	96.85	5.014	0.428	0.923	11.719	<.001	4.131	5.897		At t=0, Veq≠0
PAH	BIP	Double	0.469	57.5	191.3	25.79	7.417	<.001	138	244.5	3.386	0.736	0.685	4.6	<.001	1.867	4.906		At t=0, Veq≠0
PAH	NAP	Double	0.106	66.27	411.5	29.72	13.85	<.001	350.2	472.9	-1.435	0.849	-0.326	-1.691	0.104	-3.186	0.317		At t=0, Veq≠0
PCB	PCB 153	Double																	Insufficient detection

Cmpd class	Compound	Bowl	Regression		Constant						Slope							SR	Reason for invalid SR
			R^2	Std. Error of the Estimate	B	Std. Error of constant	t	Sig. of constant	95% CI LB of constant	95% CI UB of constant	Slope	Std. Error of slope	Std. slope	t	Sig. of slope	95% LB of slope	95% UB of slope		
HBCDD	g-HBCDD	Double	0	53.22	44.93	23.38	1.922	0.066	-3.226	93.08	-0.01	0.676	-0.003	-0.014	0.989	-1.401	1.382		Non-significant relationship between V_{eq} and deployment time
HBCDD	a-HBCDD	Double	0.008	53.78	46.24	23.62	1.957	0.062	-2.413	94.89	-0.312	0.683	-0.091	-0.457	0.651	-1.718	1.094		Non-significant relationship between V_{eq} and deployment time
HBCDD	b-HBCDD	Double	0.011	45.02	38.63	19.78	1.953	0.062	-2.105	79.37	-0.301	0.571	-0.105	-0.526	0.603	-1.478	0.876		Non-significant relationship between V_{eq} and deployment time
NHFR	DBDPE	Double	0.058	11905	4090	5230	0.782	0.442	-6681	14861	187.5	151.1	0.241	1.241	0.226	-123.756	498.686		Non-significant relationship between V_{eq} and deployment time
NHFR	BEH-TEBP	Double	0.003	128.1	65.67	56.26	1.167	0.254	-50.2	181.5	0.412	1.626	0.051	0.253	0.802	-2.936	3.76		Non-significant relationship between V_{eq} and deployment time
NHFR	BTBPE	Double	0.014	456.2	515	200.4	2.57	0.017	102.3	927.7	3.493	5.79	0.12	0.603	0.552	-8.432	15.418		Non-significant relationship between V_{eq} and deployment time
OPE	TIPPP	Double	0.084	6.218	19.67	2.752	7.147	<.001	13.99	25.35	0.117	0.079	0.29	1.485	0.15	-0.046	0.28		Non-significant relationship between V_{eq} and deployment time
OPE	TmTP	Double	0.051	10.73	26.9	4.853	5.542	<.001	16.86	36.94	0.152	0.138	0.225	1.107	0.28	-0.132	0.437		Non-significant relationship between V_{eq} and deployment time
PAH	BNT	Double	0.099	16.01	13.72	7.18	1.911	0.068	-1.095	28.54	0.334	0.205	0.315	1.627	0.117	-0.089	0.757		Non-significant relationship between V_{eq} and deployment time
PAH	BghiP	Double	0.052	0.516	0.909	0.231	3.932	<.001	0.432	1.386	-0.008	0.007	-0.228	-1.147	0.263	-0.021	0.006		Non-significant relationship between V_{eq} and deployment time

Cmpd class	Compound	Bowl	Regression		Constant						Slope							SR	Reason for invalid SR
			R^2	Std. Error of the Estimate	B	Std. Error of constant	t	Sig. of constant	95% CI LB of constant	95% CI UB of constant	Slope	Std. Error of slope	Std. slope	t	Sig. of slope	95% LB of slope	95% UB of slope		
PAH	BeP	Double	0.045	2.345	2.695	1.052	2.563	0.017	0.525	4.865	0.032	0.03	0.212	1.064	0.298	-0.03	0.094		Non-significant relationship between V_{eq} and deployment time
PAH	BAA	Double	0.011	11.07	11.58	4.966	2.331	0.028	1.329	21.83	0.074	0.142	0.106	0.523	0.606	-0.219	0.367		Non-significant relationship between V_{eq} and deployment time
PAH	CPD	Double	0.076	2.599	5.749	1.165	4.933	<.001	3.344	8.154	-0.047	0.033	-0.275	-1.403	0.173	-0.115	0.022		Non-significant relationship between V_{eq} and deployment time
PAH	CHR	Double	0.013	12.34	15.39	5.535	2.781	0.01	3.968	26.82	0.089	0.158	0.114	0.562	0.579	-0.237	0.415		Non-significant relationship between V_{eq} and deployment time
PAH	BghiF	Double	0	8.644	23.81	3.877	6.142	<.001	15.81	31.81	-0.007	0.111	-0.013	-0.063	0.95	-0.235	0.221		Non-significant relationship between V_{eq} and deployment time
PAH	BbFLU	Double	0.011	20.45	40.03	9.169	4.366	<.001	21.11	58.96	0.138	0.262	0.107	0.526	0.604	-0.403	0.678		Non-significant relationship between V_{eq} and deployment time
PAH	TPY	Double	0	21.08	45.18	9.453	4.78	<.001	25.67	64.69	0.022	0.27	0.016	0.081	0.936	-0.535	0.579		Non-significant relationship between V_{eq} and deployment time
PBDE	BDE-99	Double	0	44.3	41.05	21.34	1.923	0.067	-3.214	85.31	-0.036	0.69	-0.011	-0.052	0.959	-1.468	1.396		Non-significant relationship between V_{eq} and deployment time
PBDE	BDE-100	Double	0.077	351	371	154.2	2.406	0.024	53.43	688.5	6.453	4.455	0.278	1.448	0.16	-2.723	15.628		Non-significant relationship between V_{eq} and deployment time
PBDE	BDE-209	Double	0.024	1106	1290	496	2.6	0.016	265.9	2313	10.87	14.16	0.155	0.768	0.45	-18.355	40.099		Non-significant relationship between V_{eq} and deployment time

Cmpd class	Compound	Bowl	Regression		Constant						Slope							SR	Reason for invalid SR
			R^2	Std. Error of the Estimate	B	Std. Error of constant	t	Sig. of constant	95% CI LB of constant	95% CI UB of constant	Slope	Std. Error of slope	Std. slope	t	Sig. of slope	95% LB of slope	95% UB of slope		
OPE	TBOEP	Double	0.22	7.164	1.645	3.171	0.519	0.609	-4.899	8.189	0.237	0.091	0.469	2.603	0.016	0.049	0.425	0.237	
PCB	PCB 28	Double	0.717	4.051	2.139	1.78	1.202	0.241	-1.526	5.804	0.409	0.051	0.847	7.952	<.001	0.303	0.515	0.409	
NHFR	PBT	Double	0.862	2.776	-2.468	1.219	-2.024	0.054	-4.979	0.043	0.441	0.035	0.929	12.514	<.001	0.368	0.513	0.441	
PCB	PCB 52	Double	0.611	5.916	4.629	2.599	1.781	0.087	-0.724	9.981	0.471	0.075	0.782	6.268	<.001	0.316	0.625	0.471	
OPE	TCEP	Double	0.895	2.624	-1.209	1.161	-1.041	0.308	-3.606	1.188	0.476	0.033	0.946	14.267	<.001	0.407	0.544	0.476	
OCP	g-HCH	Double	0.678	6.325	1.951	2.779	0.702	0.489	-3.772	7.673	0.582	0.08	0.823	7.25	<.001	0.417	0.747	0.582	
PCB	PCB 101	Double	0.385	8.385	5.245	7.768	0.675	0.509	-11.22	21.71	0.599	0.189	0.62	3.164	0.006	0.198	1.001	0.599	
NHFR	HBB	Double	0.871	3.835	-2.602	1.685	-1.545	0.135	-6.072	0.868	0.633	0.049	0.933	12.995	<.001	0.532	0.733	0.633	
PAH	PYR	Double	0.955	2.202	-1.827	0.987	-1.85	0.077	-3.865	0.211	0.634	0.028	0.977	22.475	<.001	0.575	0.692	0.634	
PCB	PCB 11	Double	0.786	5.347	1.798	2.349	0.766	0.451	-3.039	6.636	0.65	0.068	0.886	9.576	<.001	0.51	0.79	0.65	
PAH	FLA	Double	0.796	5.372	2.417	2.409	1.003	0.326	-2.555	7.389	0.665	0.069	0.892	9.665	<.001	0.523	0.807	0.665	
NHFR	PBBZ	Double	0.884	3.878	-3.404	1.704	-1.998	0.057	-6.913	0.105	0.678	0.049	0.94	13.772	<.001	0.577	0.779	0.678	
OCP	p,p'-DDE	Double	0.539	10.06	7.241	4.418	1.639	0.114	-1.859	16.34	0.691	0.128	0.734	5.411	<.001	0.428	0.954	0.691	
NHFR	TBP-DBPE	Double	0.579	9.585	-1.189	4.21	-0.282	0.78	-9.861	7.483	0.714	0.122	0.761	5.866	<.001	0.463	0.964	0.714	
OCP	a-HCH	Double	0.761	6.333	-0.54	2.782	-0.194	0.848	-6.27	5.19	0.718	0.08	0.873	8.933	<.001	0.553	0.884	0.718	

Cmpd class	Compound	Bowl	Regression		Constant						Slope							SR	Reason for invalid SR
			R^2	Std. Error of the Estimate	B	Std. Error of constant	t	Sig. of constant	95% CI LB of constant	95% CI UB of constant	Slope	Std. Error of slope	Std. slope	t	Sig. of slope	95% LB of slope	95% UB of slope		
PAH	ANT	Double	0.962	2.353	-0.366	1.055	-0.347	0.732	-2.544	1.811	0.742	0.03	0.981	24.634	<.001	0.68	0.804	0.742	
OPE	EHDPP	Double	0.855	4.944	-0.61	2.188	-0.279	0.783	-5.126	3.906	0.747	0.063	0.925	11.898	<.001	0.618	0.877	0.747	
PAH	RET	Double	0.748	7.349	-1.595	3.296	-0.484	0.633	-8.397	5.206	0.794	0.094	0.865	8.438	<.001	0.6	0.988	0.794	
PAH	PHE	Double	0.959	2.631	-1.506	1.18	-1.276	0.214	-3.941	0.929	0.799	0.034	0.979	23.73	<.001	0.73	0.869	0.799	
OPE	TiBP	Double	0.912	4.31	-0.93	1.907	-0.488	0.63	-4.867	3.006	0.862	0.055	0.955	15.741	<.001	0.749	0.975	0.862	
PCB	PCB 9	Double	0.727	4.66	11.4	7.936	1.436	0.181	-6.285	29.08	0.888	0.172	0.853	5.165	<.001	0.505	1.271	0.888	
OPE	TnBP	Double	0.272	27	4.949	11.95	0.414	0.682	-19.71	29.61	1.026	0.343	0.521	2.992	0.006	0.318	1.734	1.026	
OPE	DBPP	Double	0.924	5.427	-1.299	2.402	-0.541	0.594	-6.256	3.659	1.18	0.069	0.961	17.119	<.001	1.038	1.323	1.18	
PBDE	BDE-47	Double	0.154	54.09	19.35	26.06	0.742	0.466	-34.7	73.39	1.687	0.843	0.392	2.002	0.058	-0.061	3.436	1.687	
NHFR	BATE	Double	0.602	26.81	20.86	11.78	1.771	0.089	-3.396	45.12	2.091	0.34	0.776	6.145	<.001	1.39	2.792	2.091	
OCP	HCB	Double	0.745	21.54	12.23	9.461	1.292	0.208	-7.259	31.71	2.337	0.273	0.863	8.55	<.001	1.774	2.9	2.337	
OCP	PeCB	Double	0.338	73.35	55.27	32.22	1.715	0.099	-11.1	121.6	3.328	0.931	0.582	3.575	0.001	1.411	5.246	3.328	
NHFR	EH-TBB	Double	0.324	121	-13.19	53.15	-0.248	0.806	-122.7	96.27	5.316	1.536	0.569	3.462	0.002	2.153	8.479	5.316	
NHFR	BATE	Single	0.193	78.13	283.4	34.32	8.258	<.001	212.8	354.1	-2.428	0.992	-0.44	-2.448	0.022	-4.47	-0.385		At t=0, Veq≠0
OCP	HCB	Single	0.948	14.6	32.94	6.414	5.135	<.001	19.73	46.15	3.955	0.185	0.974	21.339	<.001	3.573	4.336		At t=0, Veq≠0

Cmpd class	Compound	Bowl	Regression		Constant						Slope							SR	Reason for invalid SR
			R^2	Std. Error of the Estimate	B	Std. Error of constant	t	Sig. of constant	95% CI LB of constant	95% CI UB of constant	Slope	Std. Error of slope	Std. slope	t	Sig. of slope	95% LB of slope	95% UB of slope		
OCP	PeCB	Single	0.832	27.6	119.1	12.13	9.82	<.001	94.09	144	3.894	0.35	0.912	11.115	<.001	3.172	4.615		At t=0, Veq≠0
OPE	BDPP	Single	0.858	25.25	-31.87	11.09	-2.874	0.008	-54.71	-9.028	3.931	0.32	0.926	12.267	<.001	3.271	4.591		At t=0, Veq≠0
OPE	TPhP	Single	0.907	11.01	13.5	4.838	2.79	0.01	3.534	23.46	2.178	0.14	0.952	15.578	<.001	1.89	2.466		At t=0, Veq≠0
PAH	CHR	Single	0.449	10.24	9.952	4.497	2.213	0.036	0.691	19.21	0.587	0.13	0.67	4.518	<.001	0.319	0.855		At t=0, Veq≠0
PAH	PHE	Single	0.979	3.43	3.868	1.507	2.568	0.017	0.765	6.971	1.479	0.044	0.989	33.975	<.001	1.389	1.569		At t=0, Veq≠0
PAH	TPY	Single	0.424	28	26.63	12.3	2.165	0.04	1.295	51.97	1.526	0.355	0.651	4.292	<.001	0.793	2.258		At t=0, Veq≠0
PAH	BBF	Single	0.121	3.342	11.15	1.468	7.592	<.001	8.122	14.17	-0.079	0.042	-0.348	-1.855	0.075	-0.166	0.009		At t=0, Veq≠0
PAH	BghiF	Single	0.162	16.47	30.36	7.236	4.196	<.001	15.46	45.27	0.459	0.209	0.402	2.195	0.038	0.028	0.889		At t=0, Veq≠0
PAH	BbFLU	Single	0.172	50.76	62.15	22.3	2.788	0.01	16.23	108.1	1.468	0.644	0.415	2.279	0.031	0.141	2.795		At t=0, Veq≠0
PAH	FLU	Single	0.914	15.04	48.29	6.605	7.311	<.001	34.69	61.9	3.107	0.191	0.956	16.282	<.001	2.714	3.501		At t=0, Veq≠0
PAH	ACY	Single	0.863	38.93	146.9	17.1	8.588	<.001	111.6	182.1	6.188	0.494	0.929	12.525	<.001	5.171	7.206		At t=0, Veq≠0
PAH	ACE	Single	0.753	42.23	161.4	18.55	8.699	<.001	123.2	199.6	4.684	0.536	0.868	8.739	<.001	3.58	5.788		At t=0, Veq≠0
NHFR	DBDPE	Single	0.051	34028	-1751	14948	-0.117	0.908	-32538	29036	502.4	431.9	0.227	1.163	0.256	-387.193	1391.943		Non-significant relationship between V_{eq} and deployment time
NHFR	EH-TBB	Single	0.066	515.3	203.2	226.4	0.898	0.378	-263	669.4	8.714	6.541	0.257	1.332	0.195	-4.756	22.185		Non-significant relationship between V_{eq} and deployment time

Cmpd class	Compound	Bowl	Regression		Constant						Slope							SR	Reason for invalid SR
			R^2	Std. Error of the Estimate	B	Std. Error of constant	t	Sig. of constant	95% CI LB of constant	95% CI UB of constant	Slope	Std. Error of slope	Std. slope	t	Sig. of slope	95% LB of slope	95% UB of slope		
OPE	TCIPP	Single	0.016	52.37	131.4	23	5.713	<.001	84.04	178.8	0.417	0.665	0.125	0.628	0.536	-0.952	1.786		Non-significant relationship between V_{eq} and deployment time
PAH	IDP	Single	0.054	1.432	1.665	0.629	2.646	0.014	0.369	2.96	0.022	0.018	0.231	1.19	0.245	-0.016	0.059		Non-significant relationship between V_{eq} and deployment time
PAH	BjF	Single	0.01	3.078	5.038	1.352	3.726	<.001	2.253	7.822	-0.02	0.039	-0.102	-0.513	0.613	-0.1	0.06		Non-significant relationship between V_{eq} and deployment time
PAH	BKF	Single	0.014	2.623	5.54	1.152	4.808	<.001	3.167	7.914	-0.02	0.033	-0.12	-0.602	0.552	-0.089	0.049		Non-significant relationship between V_{eq} and deployment time
PAH	BIP	Single	0.05	55.36	342.4	24.32	14.08	<.001	292.3	392.4	0.809	0.703	0.224	1.152	0.26	-0.638	2.256		Non-significant relationship between V_{eq} and deployment time
PAH	NAP	Single	0.044	79.26	427.7	34.82	12.28	<.001	356	499.4	-1.079	1.006	-0.21	-1.073	0.294	-3.151	0.993		Non-significant relationship between V_{eq} and deployment time
PBDE	BDE-99	Single	0.072	36.38	20.8	17.53	1.187	0.248	-15.55	57.15	0.74	0.567	0.268	1.305	0.205	-0.436	1.916		Non-significant relationship between V_{eq} and deployment time
PBDE	BDE-209	Single	0	870.5	1743	382.4	4.558	<.001	955.5	2531	-0.009	11.05	0	-0.001	0.999	-22.765	22.746		Non-significant relationship between V_{eq} and deployment time
PAH	BghiP	Single	0.136	0.481	0.822	0.211	3.894	<.001	0.387	1.257	0.012	0.006	0.368	1.981	0.059	0	0.025	0.012	
PAH	CPD	Single	0.251	4.148	3.761	1.822	2.064	0.05	0.008	7.515	0.152	0.053	0.501	2.893	0.008	0.044	0.261	0.152	
PAH	ANT	Single	0.964	4.027	4.016	1.769	2.27	0.032	0.373	7.66	1.329	0.051	0.982	26.004	<.001	1.224	1.434	1.329	

Cmpd class	Compound	Bowl	Regression		Constant						Slope							SR	Reason for invalid SR
			R^2	Std. Error of the Estimate	B	Std. Error of constant	t	Sig. of constant	95% CI LB of constant	95% CI UB of constant	Slope	Std. Error of slope	Std. slope	t	Sig. of slope	95% LB of slope	95% UB of slope		
PAH	BeP	Single	0.422	2.835	0.835	1.245	0.671	0.509	-1.73	3.4	0.154	0.036	0.65	4.272	<.001	0.08	0.228	0.154	
HBCDD	b-HBCDD	Single	0.175	14.56	3.894	6.398	0.609	0.548	-9.282	17.07	0.425	0.185	0.418	2.3	0.03	0.044	0.806	0.425	
PAH	BAA	Single	0.334	10.59	9.555	4.652	2.054	0.051	-0.026	19.14	0.476	0.134	0.578	3.543	0.002	0.199	0.753	0.476	
HBCDD	a-HBCDD	Single	0.23	16.82	4.404	7.387	0.596	0.556	-10.81	19.62	0.584	0.213	0.48	2.735	0.011	0.144	1.023	0.584	
HBCDD	g-HBCDD	Single	0.202	21.06	8.731	9.252	0.944	0.354	-10.32	27.79	0.673	0.267	0.45	2.518	0.019	0.123	1.224	0.673	
OPE	TBOEP	Single	0.789	5.743	-2.279	2.523	-0.904	0.375	-7.475	2.916	0.705	0.073	0.888	9.677	<.001	0.555	0.856	0.705	
PCB	PCB 28	Single	0.91	4.638	-0.111	2.037	-0.055	0.957	-4.307	4.085	0.937	0.059	0.954	15.92	<.001	0.816	1.058	0.937	
NHFR	PBT	Single	0.892	5.455	-1.671	2.396	-0.697	0.492	-6.607	3.264	0.996	0.069	0.945	14.385	<.001	0.853	1.139	0.996	
OPE	TmTP	Single	0.68	11.05	7.826	4.856	1.612	0.12	-2.174	17.83	1.022	0.14	0.824	7.282	<.001	0.733	1.311	1.022	
OPE	TIPPP	Single	0.876	6.142	3.691	2.698	1.368	0.184	-1.867	9.248	1.036	0.078	0.936	13.284	<.001	0.875	1.196	1.036	
PAH	BNT	Single	0.837	8.116	-1.409	3.566	-0.395	0.696	-8.752	5.935	1.169	0.103	0.915	11.344	<.001	0.957	1.381	1.169	
PCB	PCB 52	Single	0.935	4.894	0.115	2.15	0.054	0.958	-4.313	4.544	1.175	0.062	0.967	18.912	<.001	1.047	1.303	1.175	
OCP	g-HCH	Single	0.907	6.256	1.093	2.748	0.398	0.694	-4.567	6.752	1.237	0.079	0.952	15.581	<.001	1.074	1.401	1.237	
PCB	PCB 101	Single	0.794	8.792	3.45	4.943	0.698	0.493	-6.801	13.7	1.244	0.135	0.891	9.218	<.001	0.964	1.524	1.244	

			Regression		Constant						Slope								
Cmpd class	**Compound**	**Bowl**	**R^2**	**Std. Error of the Estimate**	**B**	**Std. Error of constant**	**t**	**Sig. of constant**	**95% CI LB of constant**	**95% CI UB of constant**	**Slope**	**Std. Error of slope**	**Std. slope**	**t**	**Sig. of slope**	**95% LB of slope**	**95% UB of slope**	**SR**	**Reason for invalid SR**
NHFR	HBB	Single	0.836	8.709	7.931	3.826	2.073	0.049	0.051	15.81	1.247	0.111	0.914	11.283	<.001	1.02	1.475	1.247	
OPE	TnBP	Single	0.811	9.793	9.08	4.302	2.111	0.045	0.22	17.94	1.289	0.124	0.901	10.367	<.001	1.033	1.545	1.289	
OCP	a-HCH	Single	0.841	8.966	3.518	3.939	0.893	0.38	-4.594	11.63	1.308	0.114	0.917	11.491	<.001	1.073	1.542	1.308	
PAH	PYR	Single	0.941	5.202	0.228	2.285	0.1	0.921	-4.479	4.934	1.317	0.066	0.97	19.938	<.001	1.181	1.453	1.317	
OPE	TCEP	Single	0.925	6.037	0.24	2.652	0.09	0.929	-5.222	5.701	1.346	0.077	0.962	17.569	<.001	1.188	1.504	1.346	
NHFR	PBBZ	Single	0.92	6.256	1.929	2.748	0.702	0.489	-3.731	7.589	1.348	0.079	0.959	16.978	<.001	1.185	1.512	1.348	
PCB	PCB 11	Single	0.943	5.347	1.797	2.349	0.765	0.451	-3.041	6.635	1.387	0.068	0.971	20.43	<.001	1.247	1.526	1.387	
PAH	FLA	Single	0.91	6.872	5.276	3.019	1.748	0.093	-0.941	11.49	1.391	0.087	0.954	15.947	<.001	1.211	1.571	1.391	
OPE	TiBP	Single	0.907	7.494	3.532	3.292	1.073	0.294	-3.248	10.31	1.481	0.095	0.952	15.573	<.001	1.285	1.677	1.481	
OCP	p,p'-DDE	Single	0.882	8.861	5.442	3.893	1.398	0.174	-2.576	13.46	1.536	0.112	0.939	13.657	<.001	1.305	1.768	1.536	
PAH	RET	Single	0.836	11.77	-1.225	5.169	-0.237	0.815	-11.87	9.42	1.688	0.149	0.915	11.306	<.001	1.381	1.996	1.688	
HFR	TBP-DBPE	Single	0.735	16.11	-6.425	7.078	-0.908	0.373	-21	8.151	1.701	0.205	0.857	8.32	<.001	1.28	2.123	1.701	
PCB	PCB 153	Single	0.701	19.3	-16.74	8.478	-1.974	0.059	-34.2	0.722	1.874	0.245	0.837	7.65	<.001	1.37	2.379	1.874	
OPE	EHDPP	Single	0.955	7.774	-3.294	3.415	-0.965	0.344	-10.33	3.739	2.274	0.099	0.977	23.051	<.001	2.071	2.478	2.274	
PCB	PCB 9	Single	0.916	11.68	-10.43	5.132	-2.033	0.053	-21	0.138	2.454	0.148	0.957	16.548	<.001	2.148	2.759	2.454	

Cmpd class	Compound	Bowl	Regression		Constant						Slope							SR	Reason for invalid SR
			R^2	Std. Error of the Estimate	B	Std. Error of constant	t	Sig. of constant	95% CI LB of constant	95% CI UB of constant	Slope	Std. Error of slope	Std. slope	t	Sig. of slope	95% LB of slope	95% UB of slope		
OPE	DBPP	Single	0.914	12.91	-0.671	5.672	-0.118	0.907	-12.35	11.01	2.673	0.164	0.956	16.308	<.001	2.335	3.01	2.673	
PBDE	BDE-47	Single	0.408	45.89	2.298	22.11	0.104	0.918	-43.56	48.15	2.783	0.715	0.638	3.891	<.001	1.3	4.266	2.783	
NHFR	DBE-DBCH	Single	0.941	11.34	-6.269	4.983	-1.258	0.22	-16.53	3.993	2.868	0.144	0.97	19.922	<.001	2.572	3.165	2.868	
NHFR	BTBPE	Single	0.105	328	282.2	144.1	1.959	0.061	-14.5	579	7.142	4.163	0.325	1.716	0.099	-1.432	15.716	7.142	
NHFR	BEH-TEBP	Single	0.162	496.2	-24.82	218	-0.114	0.91	-473.8	424.1	13.85	6.298	0.403	2.199	0.037	0.878	26.822	13.85	
PBDE	BDE-100	Single	0.255	422.1	210.6	185.4	1.136	0.267	-171.3	592.6	15.67	5.358	0.505	2.924	0.007	4.631	26.703	15.667	
NHFR	BATE	None	0.368	72.4	116.1	35.33	3.285	0.004	42.12	190	3.755	1.128	0.607	3.328	0.004	1.394	6.117		At t=0, Veq≠0
NHFR	BTBPE	None	0.582	926.6	3352	452.1	7.415	<.001	2406	4299	-74.29	14.44	-0.763	-5.144	<.001	-104.519	-44.061		At t=0, Veq≠0
NHFR	DBDPE	None	0.699	2580	11559	1259	9.182	<.001	8924	14194	-267.3	40.21	-0.836	-6.647	<.001	-351.46	-183.122		At t=0, Veq≠0
OCP	HCB	None	0.859	25.41	34.54	12.4	2.785	0.012	8.586	60.49	4.266	0.396	0.927	10.771	<.001	3.437	5.095		At t=0, Veq≠0
OCP	PeCB	None	0.231	65.05	142.7	31.74	4.494	<.001	76.23	209.1	2.422	1.014	0.481	2.389	0.027	0.3	4.544		At t=0, Veq≠0
OPE	TBOEP	None	0.948	5.435	-8.599	2.652	-3.243	0.004	-14.15	-3.048	1.575	0.085	0.974	18.594	<.001	1.398	1.752		At t=0, Veq≠0
OPE	TIPPP	None	0.821	9.438	10.82	4.605	2.349	0.03	1.177	20.46	1.373	0.147	0.906	9.333	<.001	1.065	1.681		At t=0, Veq≠0
OPE	TCIPP	None	0.465	33.16	65.55	16.18	4.052	<.001	31.69	99.42	2.102	0.517	0.682	4.068	<.001	1.021	3.184		At t=0, Veq≠0

Cmpd class	Compound	Bowl	Regression		Constant						Slope							SR	Reason for invalid SR
			R^2	Std. Error of the Estimate	B	Std. Error of constant	t	Sig. of constant	95% CI LB of constant	95% CI UB of constant	Slope	Std. Error of slope	Std. slope	t	Sig. of slope	95% LB of slope	95% UB of slope		
PAH	BghiF	None	0.536	13.01	15.27	6.351	2.405	0.027	1.981	28.57	0.951	0.203	0.732	4.687	<.001	0.526	1.375		At t=0, Veq≠0
PAH	BAA	None	0.28	9.091	21.22	4.436	4.784	<.001	11.94	30.5	0.385	0.142	0.529	2.717	0.014	0.088	0.682		At t=0, Veq≠0
PAH	FLU	None	0.931	15.46	38.2	7.543	5.064	<.001	22.41	53.99	3.844	0.241	0.965	15.955	<.001	3.34	4.349		At t=0, Veq≠0
PAH	ACE	None	0.764	39.38	154.6	19.22	8.045	<.001	114.4	194.8	4.812	0.614	0.874	7.84	<.001	3.527	6.097		At t=0, Veq≠0
PAH	ACY	None	0.837	35.38	194.3	17.26	11.25	<.001	158.1	230.4	5.438	0.551	0.915	9.861	<.001	4.284	6.593		At t=0, Veq≠0
PAH	NAP	None	0.589	74.19	592.8	36.2	16.38	<.001	517	668.6	-6.031	1.156	-0.767	-5.216	<.001	-8.452	-3.611		At t=0, Veq≠0
PBDE	BDE-209	None	0.664	1664	7593	812	9.35	<.001	5893	9292	-159	25.94	-0.815	-6.129	<.001	-213.265	-104.684		At t=0, Veq≠0
PCB	PCB 9	None	0.49	14.64	31.77	13.89	2.288	0.04	1.772	61.77	1.349	0.382	0.7	3.534	0.004	0.524	2.174		At t=0, Veq≠0
HBCDD	g-HBCDD	None	0.061	84.82	43.53	41.39	1.052	0.306	-43.1	130.2	1.471	1.322	0.247	1.113	0.28	-1.296	4.239		Non-significant relationship between V_{eq} and deployment time
NHFR	EH-TBB	None	0.063	462.9	446	225.9	1.974	0.063	-26.84	918.8	8.126	7.216	0.25	1.126	0.274	-6.977	23.229		Non-significant relationship between V_{eq} and deployment time
NHFR	BEH-TEBP	None	0.016	211.7	198.4	103.3	1.921	0.07	-17.82	414.6	1.842	3.3	0.127	0.558	0.583	-5.065	8.749		Non-significant relationship between V_{eq} and deployment time
PAH	IDP	None	0.095	0.924	1.839	0.451	4.081	<.001	0.896	2.783	-0.02	0.014	-0.309	-1.414	0.173	-0.051	0.01		Non-significant relationship between V_{eq} and deployment time
PAH	BBF	None	0.027	1.355	8.252	0.661	12.48	<.001	6.868	9.635	0.015	0.021	0.164	0.726	0.477	-0.029	0.06		Non-significant relationship between V_{eq} and deployment time

Cmpd class	Compound	Bowl	Regression		Constant						Slope							SR	Reason for invalid SR
			R^2	Std. Error of the Estimate	B	Std. Error of constant	t	Sig. of constant	95% CI LB of constant	95% CI UB of constant	Slope	Std. Error of slope	Std. slope	t	Sig. of slope	95% LB of slope	95% UB of slope		
PAH	BIP	None	0	38.46	363.4	18.77	19.36	<.001	324.1	402.6	-0.042	0.6	-0.016	-0.07	0.945	-1.297	1.213		Non-significant relationship between V_{eq} and deployment time
PBDE	BDE-99	None	0.084	82.2	101.3	40.11	2.526	0.021	17.35	185.3	-1.695	1.281	-0.29	-1.323	0.202	-4.377	0.987		Non-significant relationship between V_{eq} and deployment time
PAH	CPD	None	0.34	3.383	3.509	1.651	2.126	0.047	0.054	6.964	0.165	0.053	0.583	3.126	0.006	0.055	0.275	0.165	
PAH	BghiP	None	0.68	0.415	0.002	0.203	0.011	0.992	-0.422	0.426	0.041	0.006	0.824	6.347	<.001	0.028	0.055	0.041	
PAH	BKF	None	0.531	1.879	1.611	0.917	1.757	0.095	-0.308	3.53	0.136	0.029	0.729	4.638	<.001	0.075	0.197	0.136	
PAH	BjF	None	0.399	2.689	2.664	1.312	2.03	0.057	-0.082	5.411	0.149	0.042	0.631	3.548	0.002	0.061	0.236	0.149	
PAH	BeP	None	0.708	2.157	0.596	1.053	0.566	0.578	-1.607	2.799	0.228	0.034	0.842	6.795	<.001	0.158	0.299	0.228	
PAH	CHR	None	0.671	10.25	3.145	5.001	0.629	0.537	-7.322	13.61	0.994	0.16	0.819	6.224	<.001	0.66	1.329	0.994	
PCB	PCB 28	None	0.804	7.649	2.174	3.732	0.582	0.567	-5.638	9.986	1.054	0.119	0.897	8.836	<.001	0.804	1.303	1.054	
NHFR	PBT	None	0.564	15.08	0.582	7.359	0.079	0.938	-14.82	15.98	1.165	0.235	0.751	4.954	<.001	0.673	1.657	1.165	
PAH	BNT	None	0.472	19.56	18.66	9.544	1.955	0.065	-1.314	38.64	1.258	0.305	0.687	4.125	<.001	0.619	1.896	1.258	
HBCDD	b-HBCDD	None	0.63	15.96	10.06	7.785	1.292	0.212	-6.236	26.35	1.416	0.249	0.794	5.693	<.001	0.895	1.936	1.416	
OCP	a-HCH	None	0.836	9.866	4.824	4.814	1.002	0.329	-5.252	14.9	1.511	0.154	0.914	9.827	<.001	1.189	1.833	1.511	
OCP	g-HCH	None	0.867	9.223	-0.91	4.501	-0.202	0.842	-10.33	8.509	1.601	0.144	0.931	11.135	<.001	1.3	1.902	1.601	
OPE	TnBP	None	0.86	9.531	1.423	4.651	0.306	0.763	-8.311	11.16	1.607	0.149	0.928	10.818	<.001	1.296	1.918	1.607	

Cmpd class	Compound	Bowl	Regression		Constant						Slope							SR	Reason for invalid SR
			R^2	Std. Error of the Estimate	B	Std. Error of constant	t	Sig. of constant	95% CI LB of constant	95% CI UB of constant	Slope	Std. Error of slope	Std. slope	t	Sig. of slope	95% LB of slope	95% UB of slope		
PCB	PCB 52	None	0.872	9.238	-1.547	4.508	-0.343	0.735	-10.98	7.888	1.637	0.144	0.934	11.369	<.001	1.336	1.939	1.637	
PCB	PCB 11	None	0.892	8.58	0.749	4.187	0.179	0.86	-8.014	9.512	1.673	0.134	0.944	12.51	<.001	1.393	1.953	1.673	
OPE	TiBP	None	0.857	10.08	1.004	4.918	0.204	0.84	-9.29	11.3	1.678	0.157	0.926	10.683	<.001	1.35	2.007	1.678	
PAH	PYR	None	0.878	9.507	1.063	4.639	0.229	0.821	-8.646	10.77	1.73	0.148	0.937	11.672	<.001	1.419	2.04	1.73	
PCB	PCB 153	None	0.615	20.2	11.07	9.856	1.123	0.275	-9.56	31.7	1.733	0.315	0.784	5.506	<.001	1.075	2.392	1.733	
PAH	ANT	None	0.918	7.639	2.892	3.728	0.776	0.447	-4.91	10.69	1.735	0.119	0.958	14.571	<.001	1.486	1.984	1.735	
NHFR	TBP-DBPE	None	0.469	28.16	11.14	13.74	0.811	0.427	-17.62	39.9	1.797	0.439	0.685	4.095	<.001	0.879	2.716	1.797	
PAH	FLA	None	0.863	10.54	2.495	5.141	0.485	0.633	-8.265	13.25	1.8	0.164	0.929	10.96	<.001	1.456	2.143	1.8	
OCP	p,p'-DDE	None	0.834	11.83	3.861	5.77	0.669	0.511	-8.217	15.94	1.804	0.184	0.913	9.786	<.001	1.418	2.19	1.804	
OPE	TmTP	None	0.749	15.38	9.4	7.506	1.252	0.226	-6.31	25.11	1.807	0.24	0.866	7.538	<.001	1.306	2.309	1.807	
PCB	PCB 101	None	0.837	12.1	-6.508	5.905	-1.102	0.284	-18.87	5.851	1.866	0.189	0.915	9.89	<.001	1.471	2.26	1.866	
PAH	PHE	None	0.947	6.666	1.178	3.253	0.362	0.721	-5.63	7.986	1.917	0.104	0.973	18.447	<.001	1.699	2.134	1.917	
PBDE	BDE-47	None	0.158	68.94	52.04	33.64	1.547	0.138	-18.37	122.5	2.032	1.075	0.398	1.891	0.074	-0.217	4.281	2.032	
PAH	RET	None	0.858	12.97	-4.595	6.33	-0.726	0.477	-17.84	8.653	2.164	0.202	0.926	10.704	<.001	1.741	2.587	2.164	
OPE	TCEP	None	0.83	14.48	-2.01	7.064	-0.285	0.779	-16.8	12.78	2.17	0.226	0.911	9.618	<.001	1.698	2.643	2.17	
NHFR	HBB	None	0.795	16.62	8.072	8.109	0.995	0.332	-8.901	25.05	2.221	0.259	0.891	8.574	<.001	1.679	2.763	2.221	

Cmpd class	Compound	Bowl	Regression		Constant						Slope							SR	Reason for invalid SR
			R^2	Std. Error of the Estimate	B	Std. Error of constant	t	Sig. of constant	95% CI LB of constant	95% CI UB of constant	Slope	Std. Error of slope	Std. slope	t	Sig. of slope	95% LB of slope	95% UB of slope		
HBCDD	a-HBCDD	None	0.689	22.49	7.148	10.97	0.651	0.523	-15.82	30.12	2.272	0.351	0.83	6.481	<.001	1.538	3.006	2.272	
HFR	PBBZ	None	0.902	11.08	-2.529	5.409	-0.468	0.645	-13.85	8.792	2.28	0.173	0.95	13.199	<.001	1.919	2.642	2.28	
PAH	BbFLU	None	0.275	58.52	45.71	28.56	1.601	0.126	-14.06	105.5	2.447	0.912	0.524	2.682	0.015	0.538	4.356	2.447	
PAH	TPY	None	0.619	31.52	26.3	15.38	1.71	0.104	-5.896	58.49	2.727	0.491	0.786	5.55	<.001	1.699	3.756	2.727	
OPE	DBPP	None	0.863	17.75	3.749	8.659	0.433	0.67	-14.38	21.87	3.03	0.277	0.929	10.954	<.001	2.451	3.609	3.03	
NHFR	DBE-DBCH	None	0.632	39.67	-14.93	19.36	-0.771	0.45	-55.45	25.59	3.532	0.618	0.795	5.711	<.001	2.238	4.826	3.532	
OPE	TPhP	None	0.889	19.25	14.82	9.395	1.577	0.131	-4.85	34.48	3.693	0.3	0.943	12.305	<.001	3.065	4.321	3.693	
OPE	EHDPP	None	0.796	28.74	-9.006	14.02	-0.642	0.528	-38.36	20.34	3.852	0.448	0.892	8.6	<.001	2.915	4.79	3.852	
OPE	BDPP	None	0.854	31.03	-17.84	15.14	-1.178	0.253	-49.53	13.85	5.104	0.484	0.924	10.553	<.001	4.092	6.117	5.104	
PBDE	BDE-100	None	0.156	321.1	244.9	156.7	1.563	0.135	-83.06	572.8	9.378	5.005	0.395	1.874	0.076	-1.098	19.854	9.378	